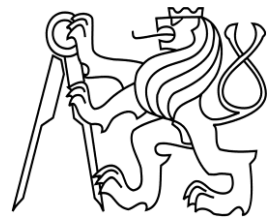


FULL-SCALE FIRE TESTING

Ing. Kamila Cábová, Ph.D.



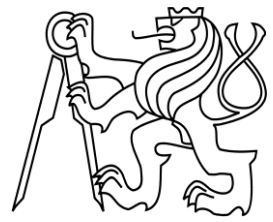
Structural fire design



Methods to define fire resistance of structures

1. Experiments
2. Tables
3. Simple models
4. Advanced models

Structural fire design

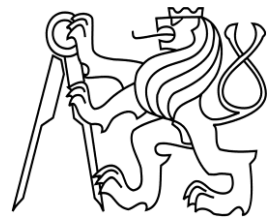


Methods to define fire resistance of structures

1. Experiments
2. Tables
3. Simple models
4. Advanced models



Experiments



- Material testing at elevated temperature
- Testing of structures
 - Standard fire testing = fire resistance testing
 - Small-scale testing of structures
 - Full-scale testing of structures



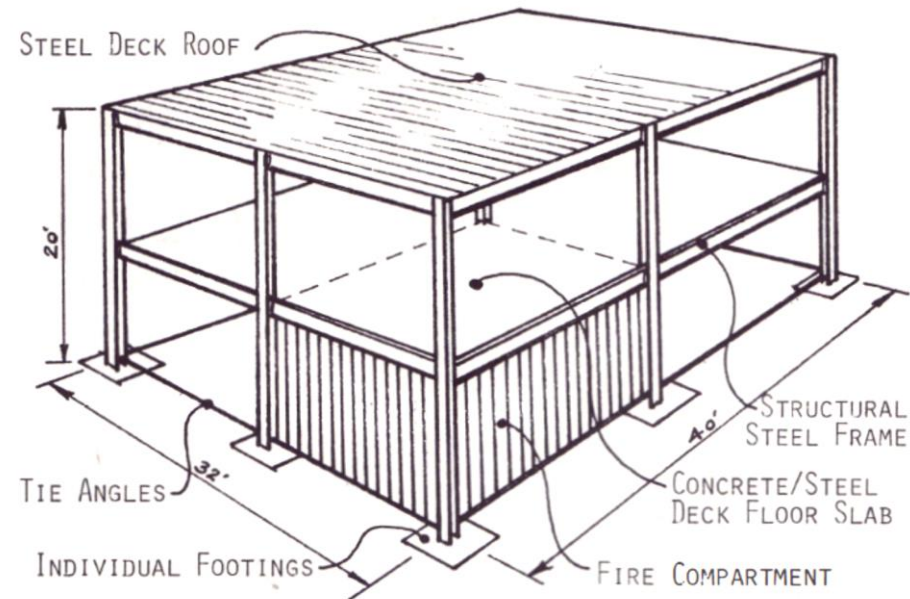
Full-scale fire testing



About 1980 a full-scale fire testing begins

1982, NIST, USA

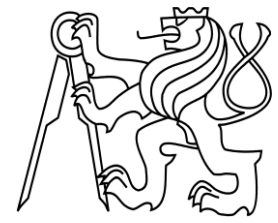
Steel-concrete composite structure



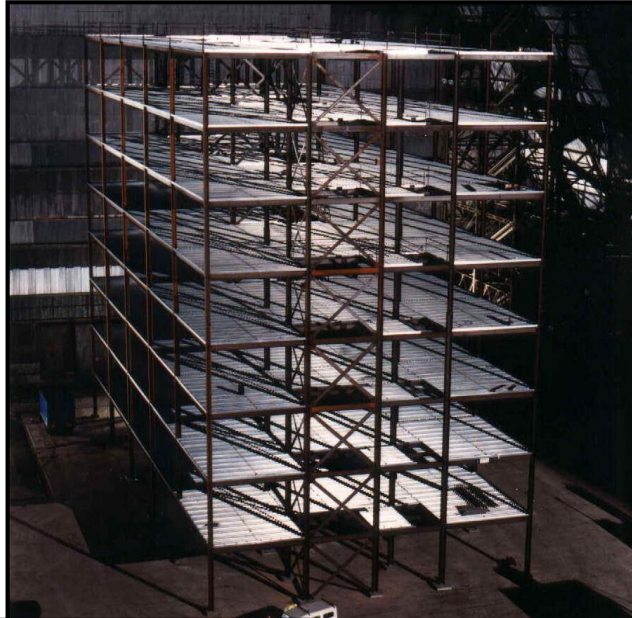
In presence about **25+** full-scale, non-standard fire tests in the literature

- Steel-concrete composite structure (≈ 20)
- Concrete (≈ 5)
- Timber (1?)

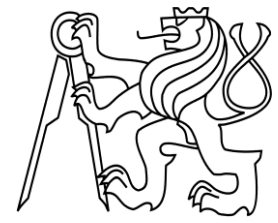
Full-scale fire testing



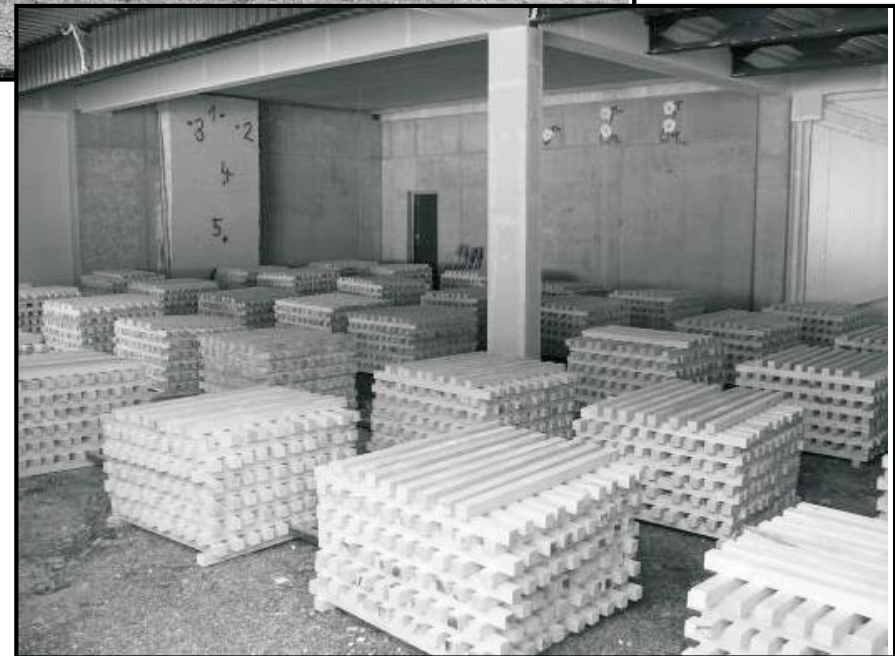
- Cardington
1995-2003



Full-scale fire testing



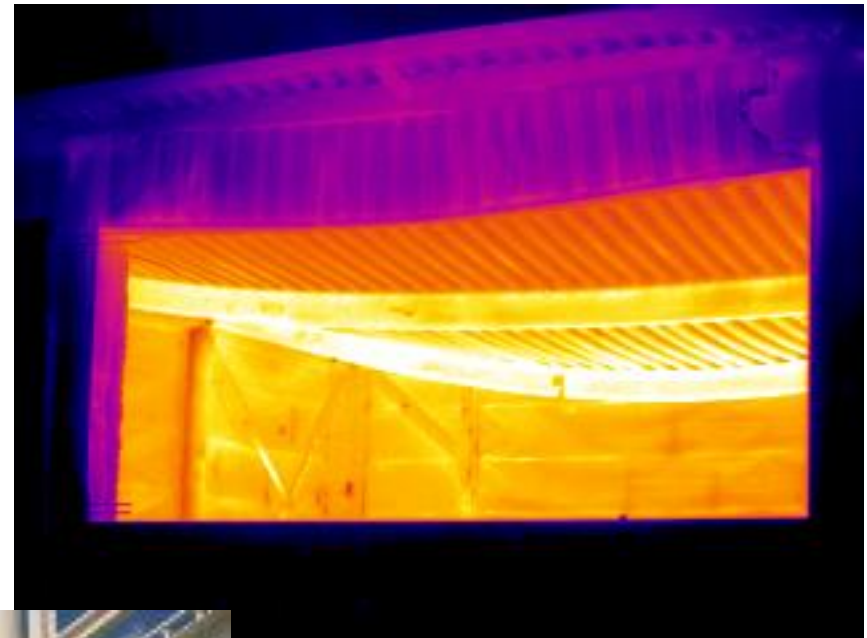
- Mokrsko, 2008



Full-scale fire testing



- Veselí n. L., 2011



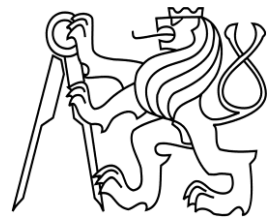
Cardington



- 8-floor composite steel-concrete building
- Fire tests between 1995 – 2003
 - Fire test organized by CTU in 2003



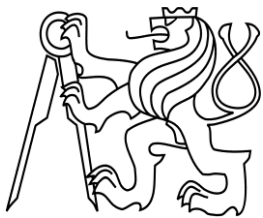
Cardington



The main building parameters

- Length - 42 m, 5 spans of 9 m
- Width - 21 m, 3 spans - 6 m, 9 m and 6 m
- Floor height – 4,2 m
- Cross-sections - imperial beams UB, columns UC
- Steel-concrete composite floor – light concrete of 130 mm in trapezoidal sheet
- Area of reinforcement of the slab of 142 mm²
- Connections
 - secondary beam to primary beam – thin plate
 - primary/secondary beam to column – end-plate
- Mechanical load – bags with sand

Cardington



Beam-to-beam connection



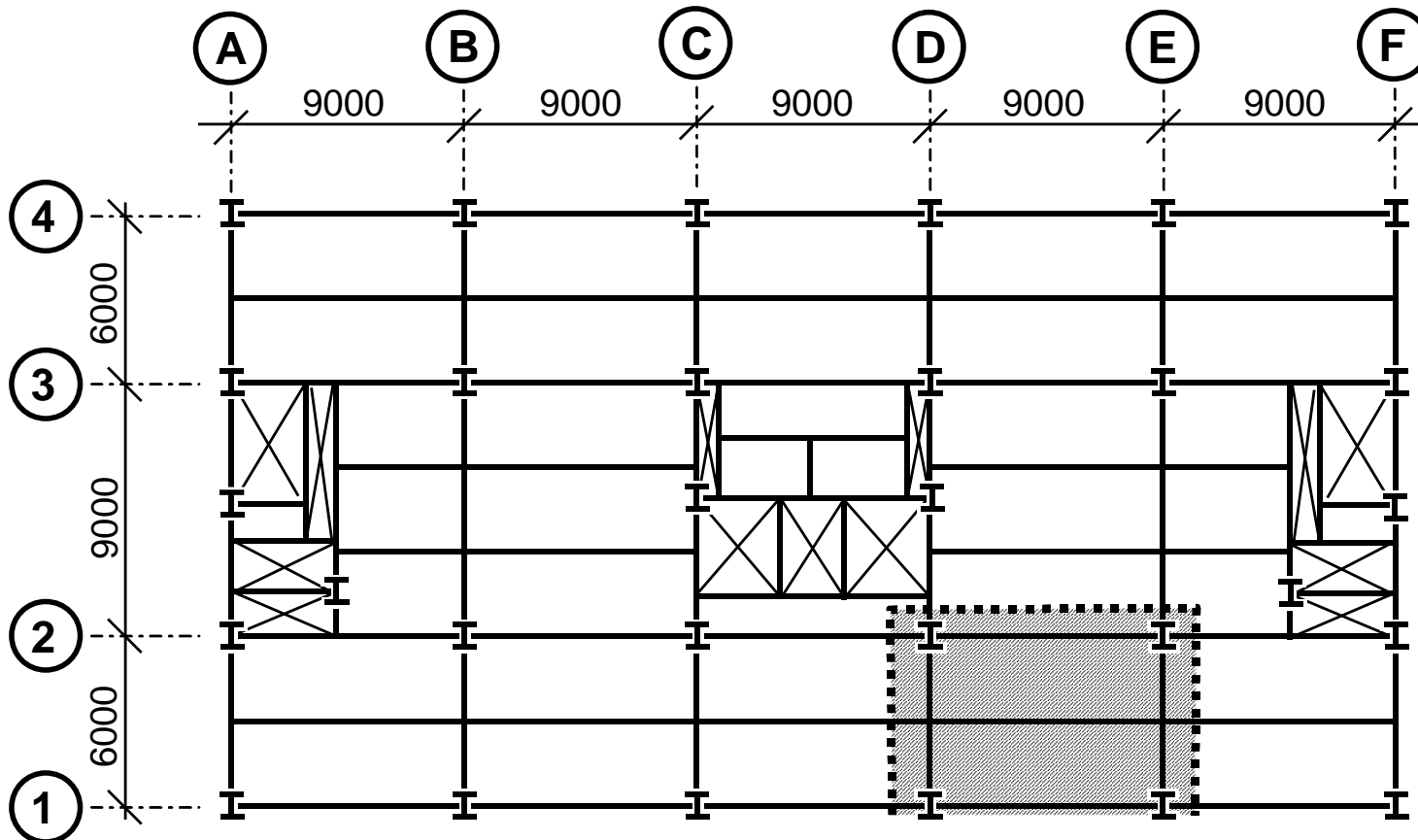
Beam-to-column connection

Cardington



Fire test of CTU

- Fire compartment

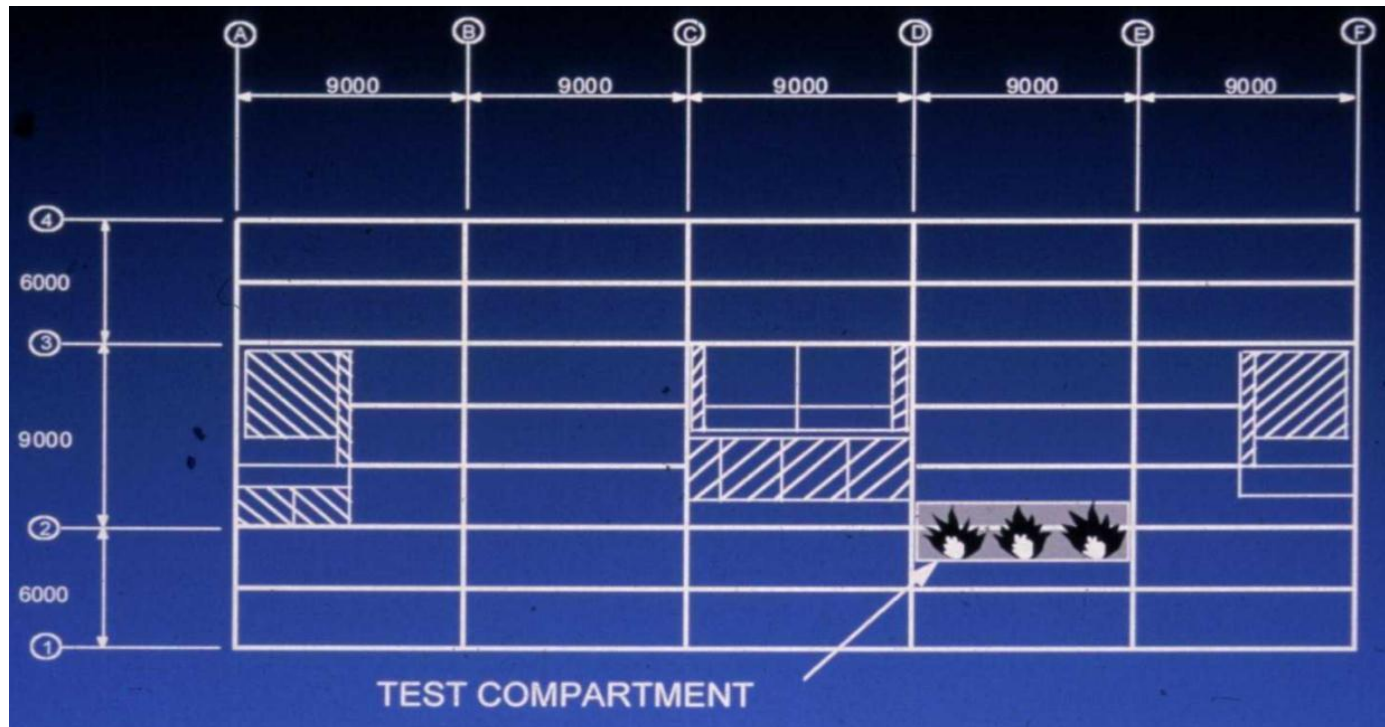


Cardington



Beam in the compartment

- Length 9,0 m
- Heating by gas burners according to standard temperature time curve

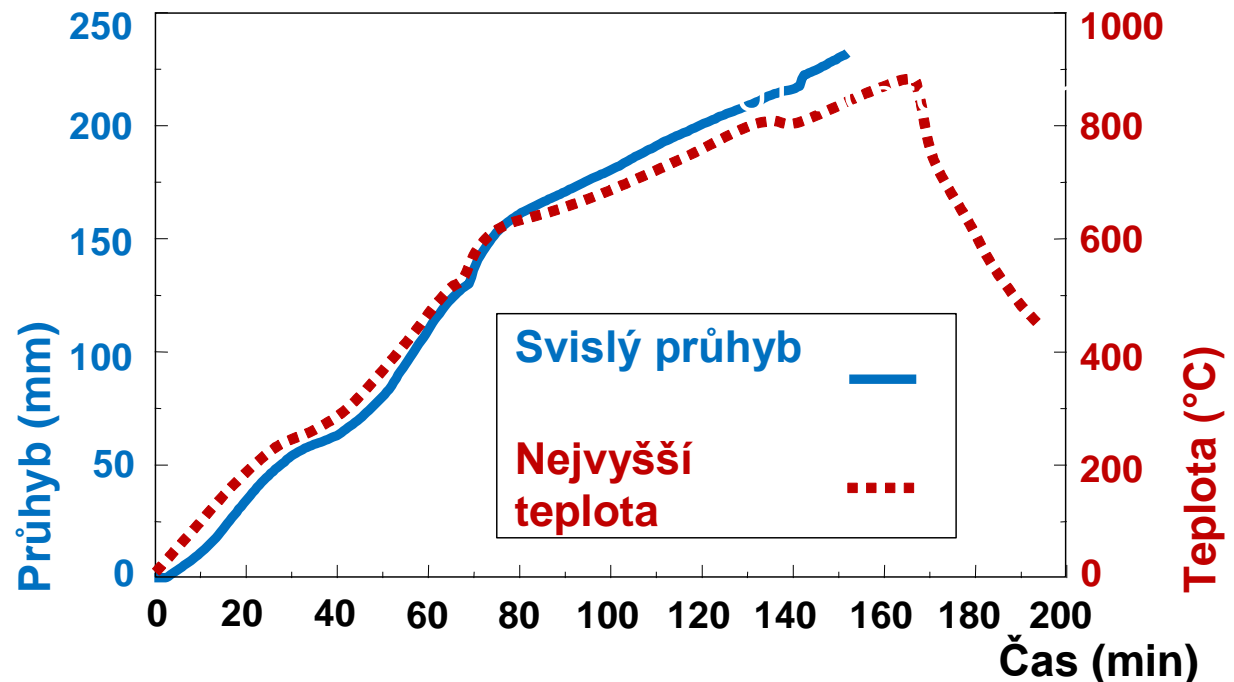


Cardington



Beam in the compartment

- Results
 - Max. temperature 900 °C
 - Beam deflection < 250 mm

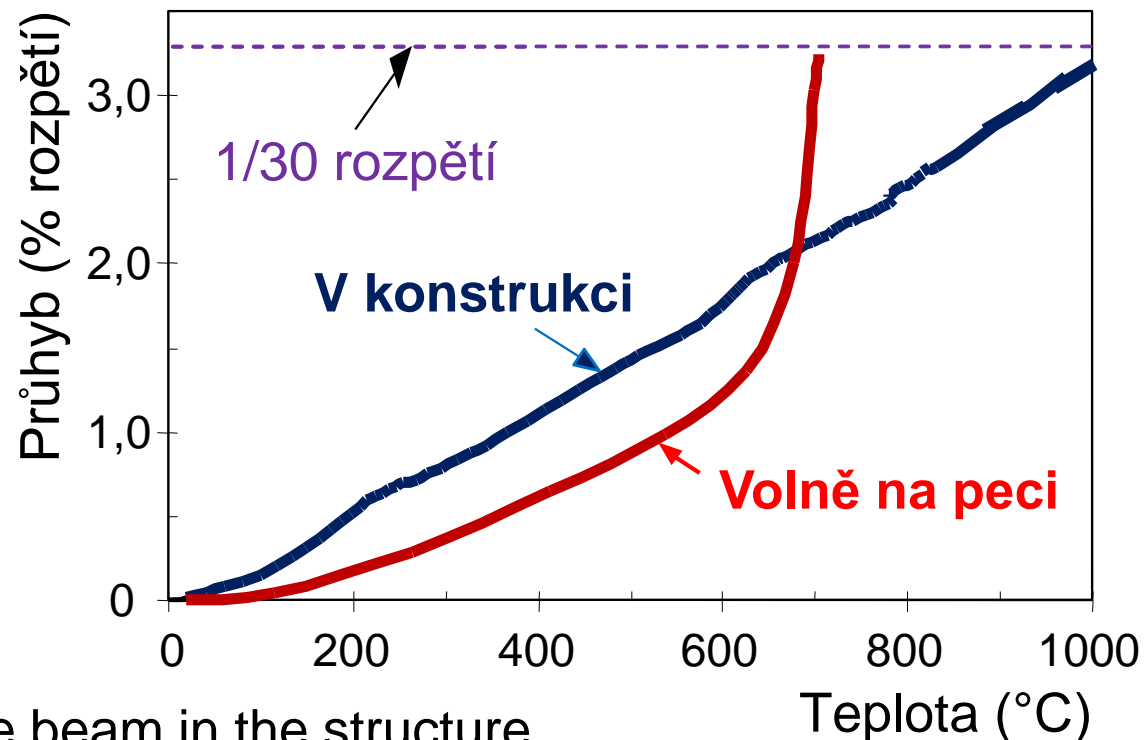


Cardington



Beam in the compartment

- Comparison of the beam deflection in the structure and deflection of a the beam tested on the horizontal furnace



- No failure of the beam in the structure
- Failure of the beam on the furnace at $\theta \approx 650$ °C

Cardington

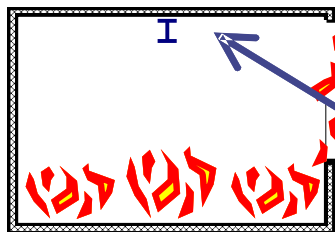


Beam-to-beam connection in the compartment



Přípoj deskou na stojně

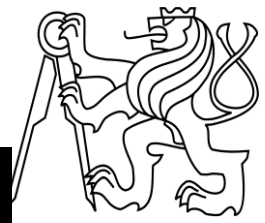
Požární úsek



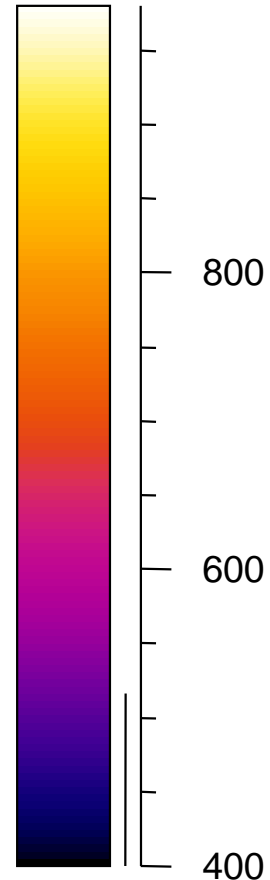
16 1 2003

$t = 26 \text{ min.}$

$\theta_{\text{con},\emptyset} = 275 \text{ }^{\circ}\text{C}$

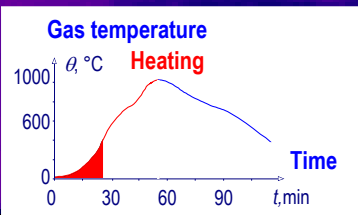
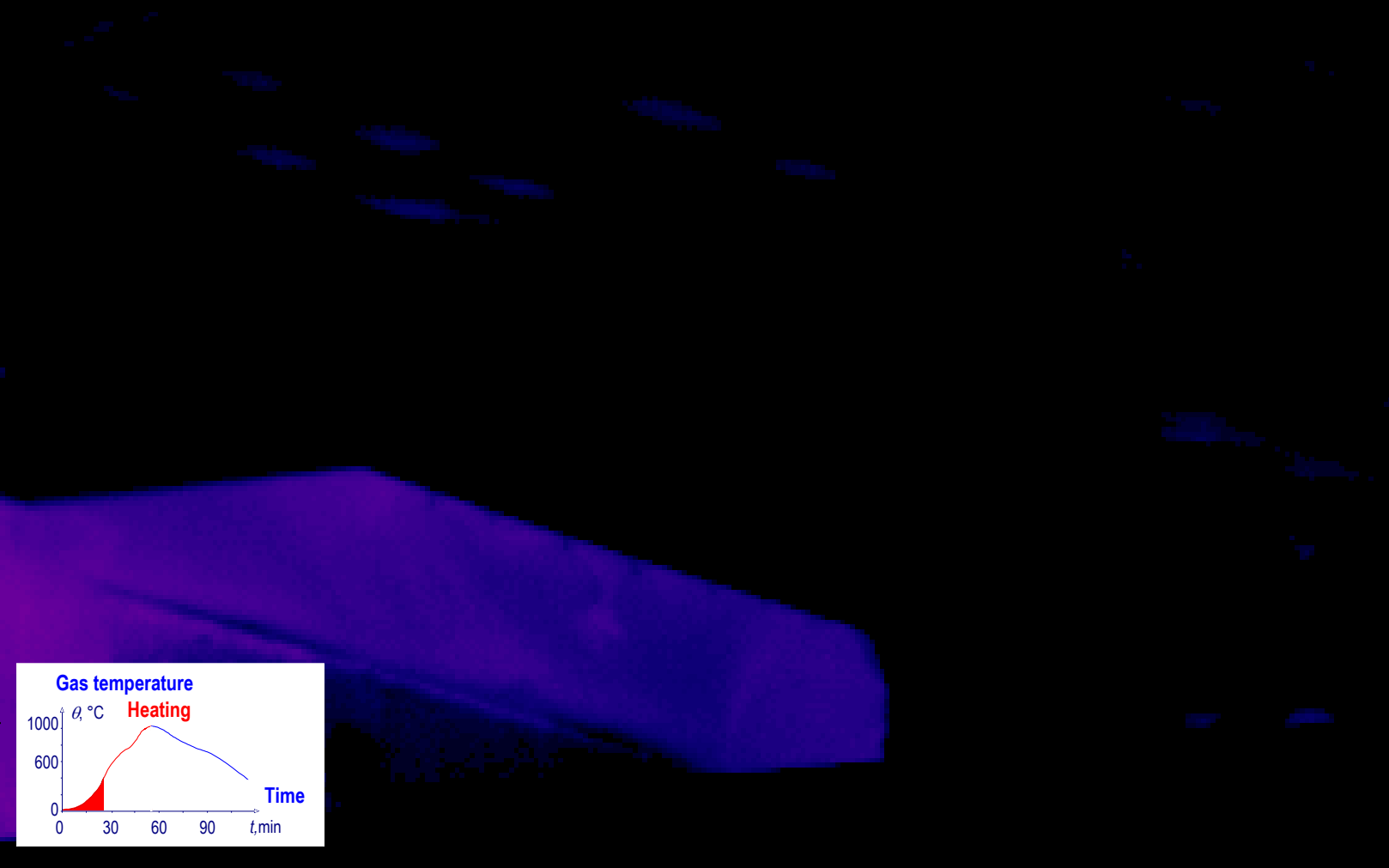


980,0°C



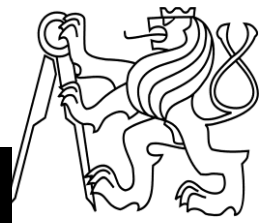
400,0°C

In 26 min of fire temperature of the structure is below 400°C

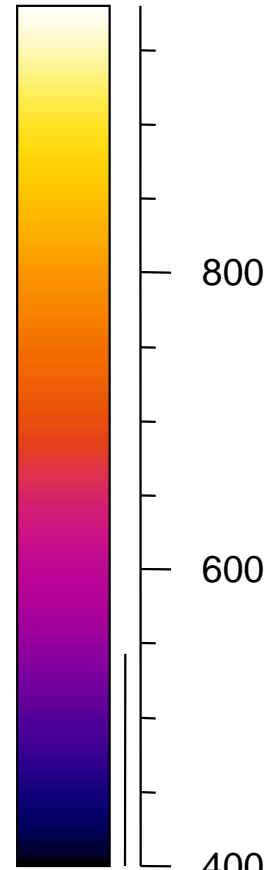
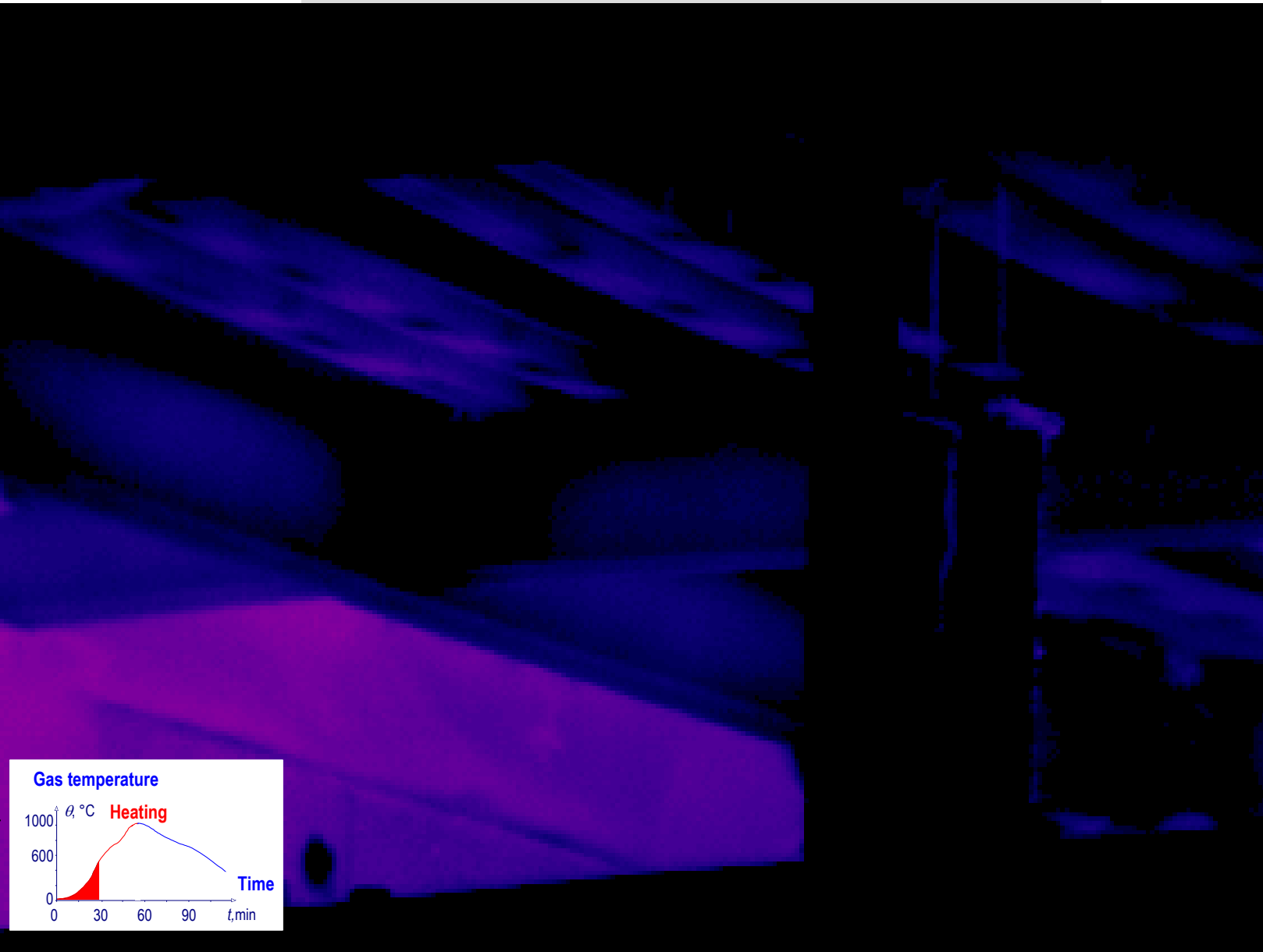


$t = 28 \text{ min.}$

$\theta_{\text{con},\vartheta} = 330 \text{ }^\circ\text{C}$

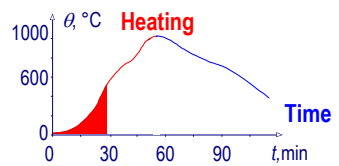


980,0°C



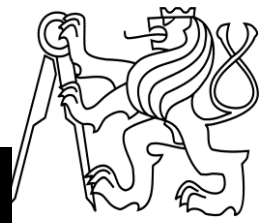
400,0°C

Gas temperature



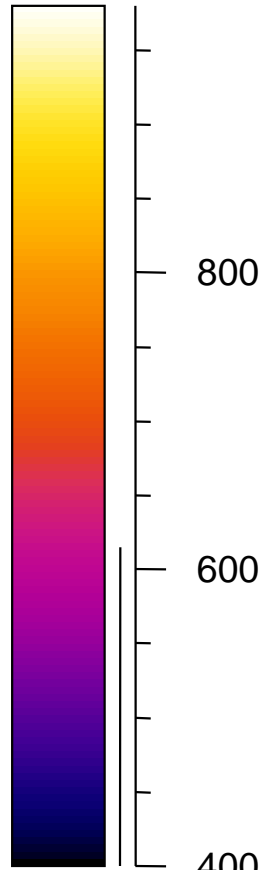
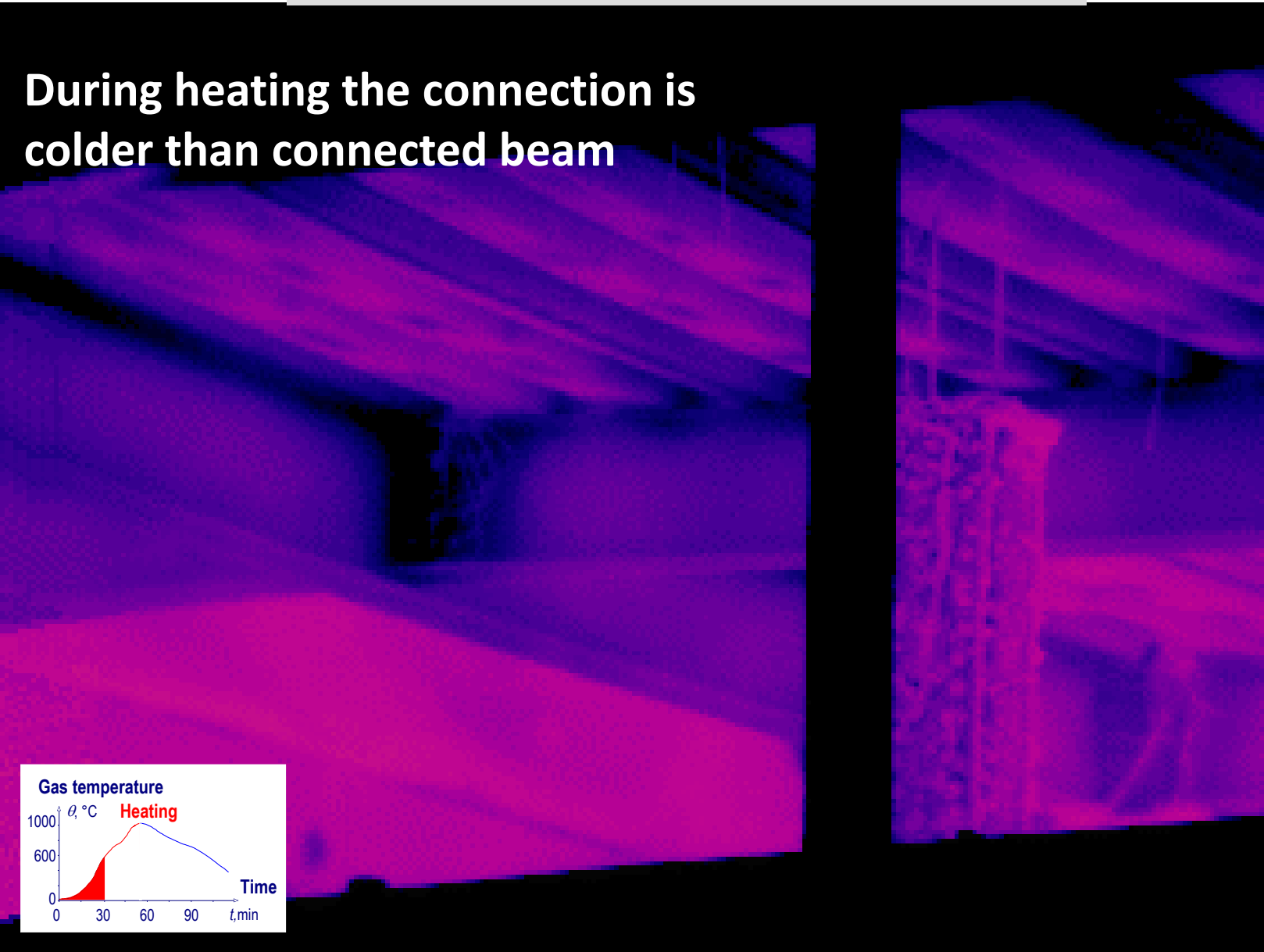
$t = 30 \text{ min.}$

$\theta_{\text{con},\theta} = 390 \text{ }^\circ\text{C}$

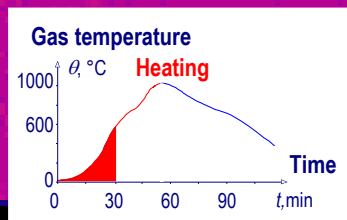


980,0°C

During heating the connection is colder than connected beam

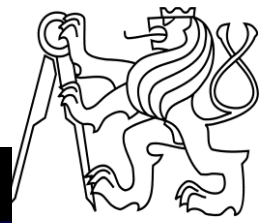


400,0°C

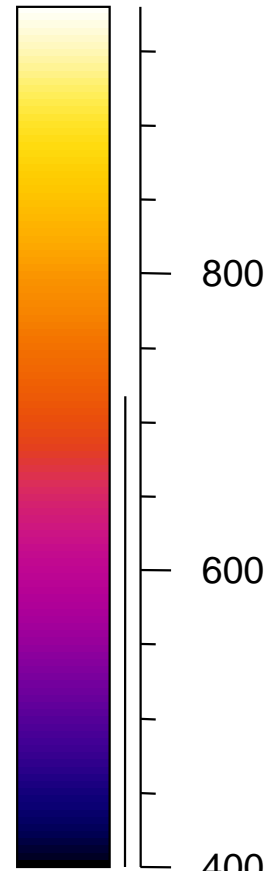


t = 32 min.

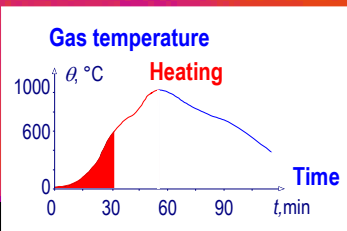
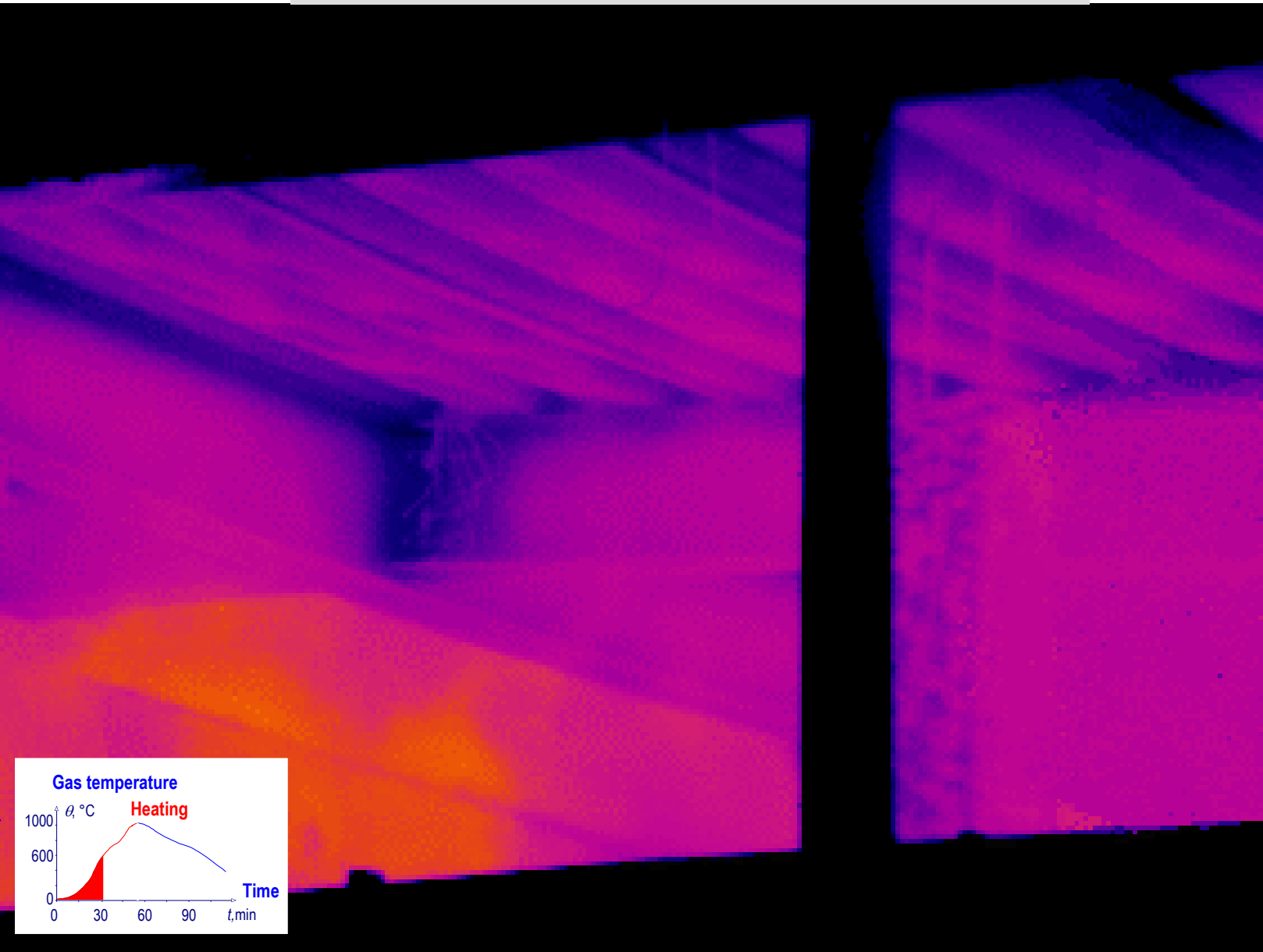
$\theta_{\text{con},\varnothing} = 440 \text{ }^{\circ}\text{C}$



980,0°C

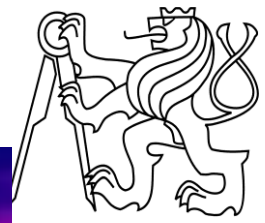


400,0°C



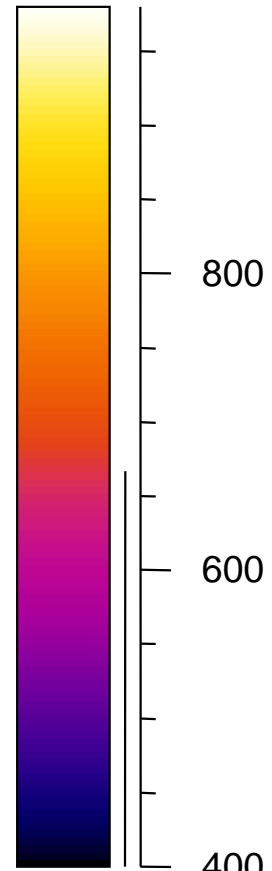
t = 34 min.

$\theta_{\text{con},\emptyset} = 480 \text{ }^\circ\text{C}$

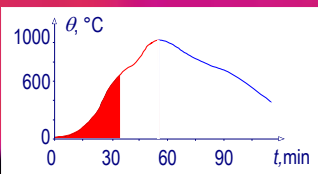


980,0°C

During heating the connection is colder than a connected beam

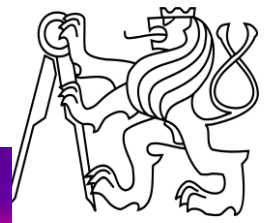


400,0°C

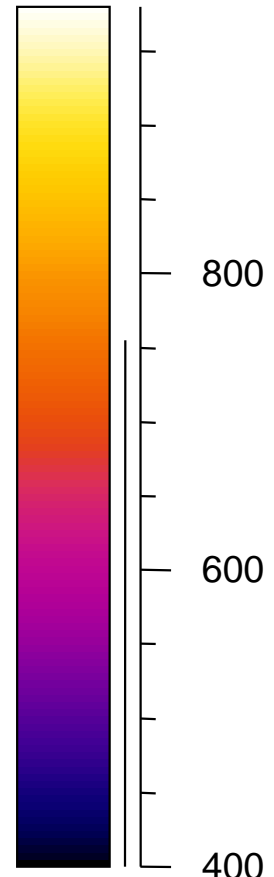


t = 36 min.

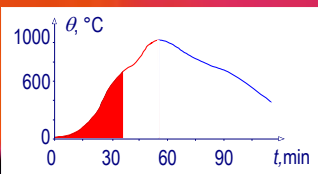
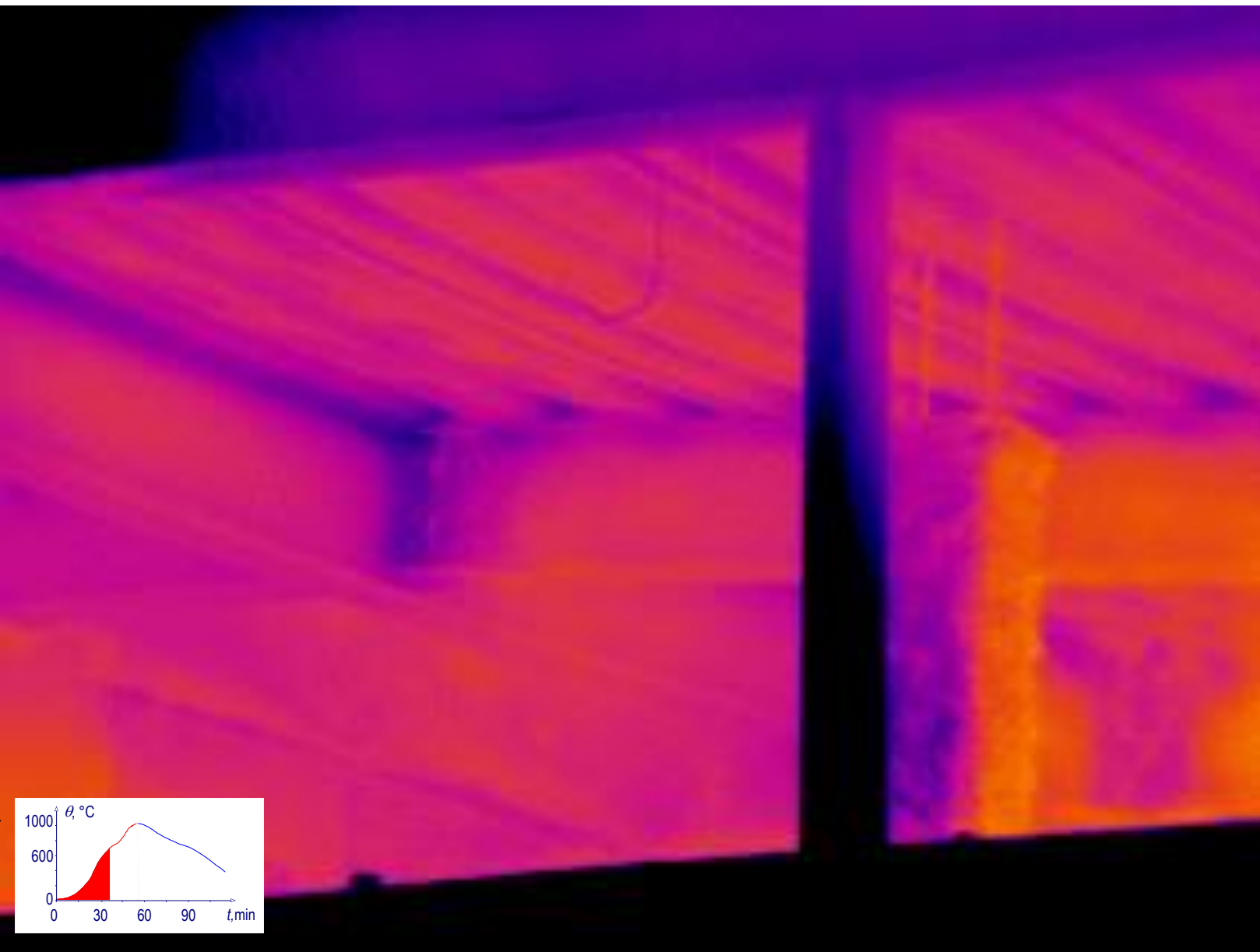
$\theta_{\text{con},\emptyset} = 520 \text{ }^\circ\text{C}$



980,0°C

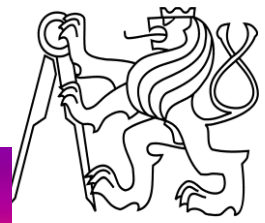


400,0°C



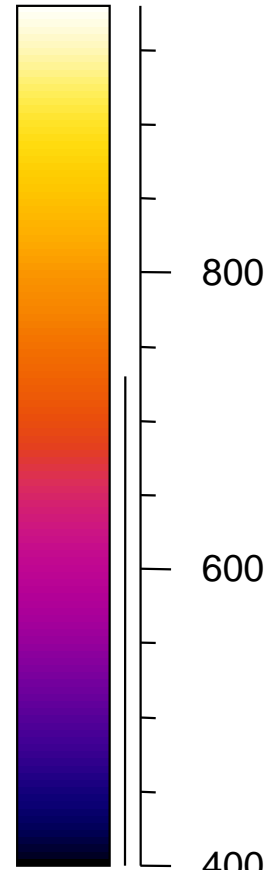
t = 38 min.

$\theta_{\text{con},\emptyset} = 565 \text{ }^\circ\text{C}$

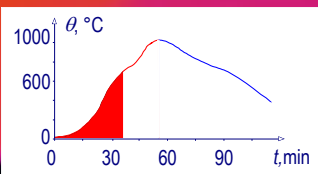


980,0°C

Buckling of the lower flange of the beam

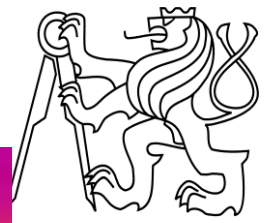


400,0°C



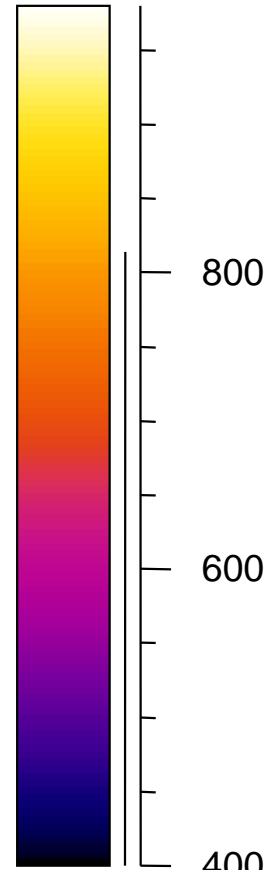
t = 40 min.

$\theta_{con,\emptyset} = 590 \text{ }^\circ\text{C}$

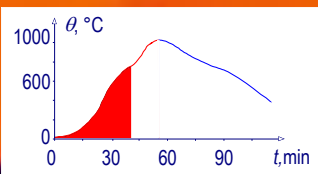


980,0°C

Buckling of the lower flange of the beam

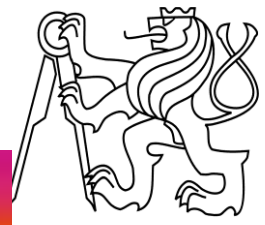


400,0°C



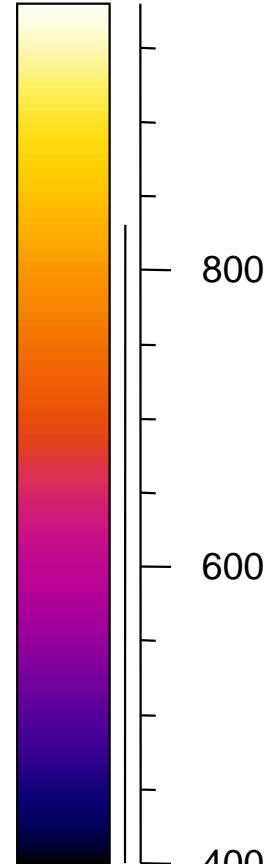
t = 42 min.

$\theta_{con,\emptyset} = 645 \text{ }^\circ\text{C}$

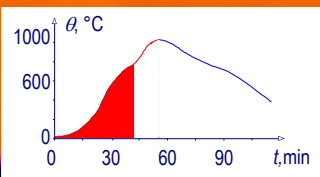


980,0°C

Buckling of the lower flange of the beam

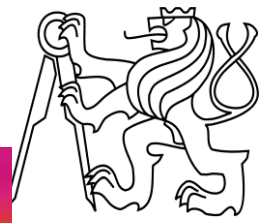


400,0°C



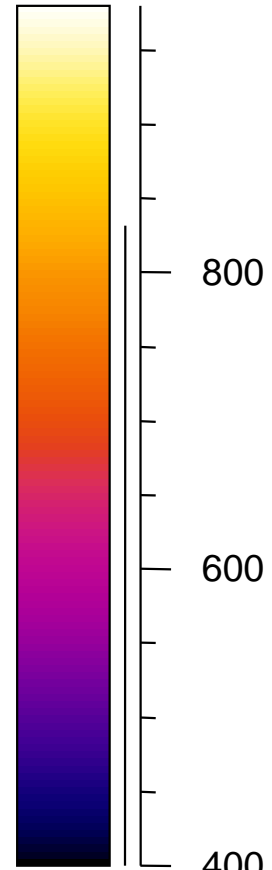
t = 44 min.

$\theta_{\text{con},\emptyset} = 660 \text{ }^{\circ}\text{C}$

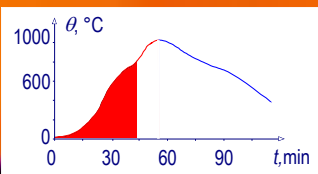


980,0°C

Buckling of the lower flange of the beam

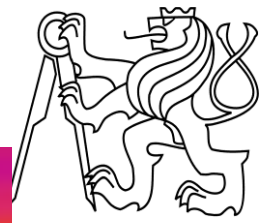


400,0°C



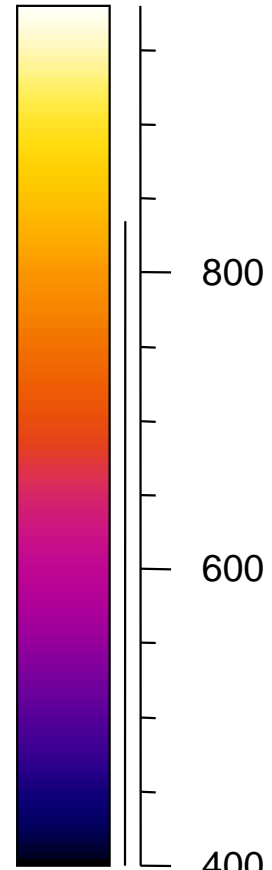
t = 46 min.

$\theta_{\text{con},\emptyset} = 685 \text{ }^\circ\text{C}$

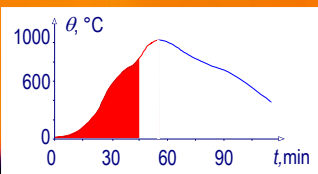


980,0°C

Buckling of the lower flange of the beam

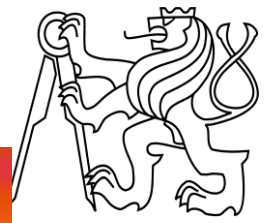


400,0°C



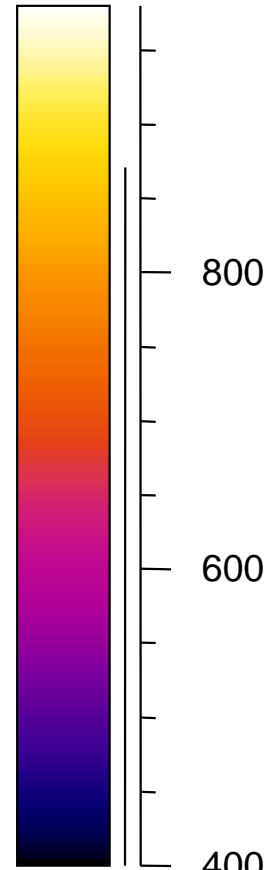
t = 48 min.

$\theta_{\text{con},\emptyset} = 710 \text{ }^{\circ}\text{C}$

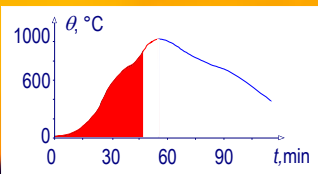


980,0°C

Buckling of the lower flange of the beam

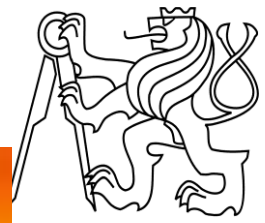


400,0°C



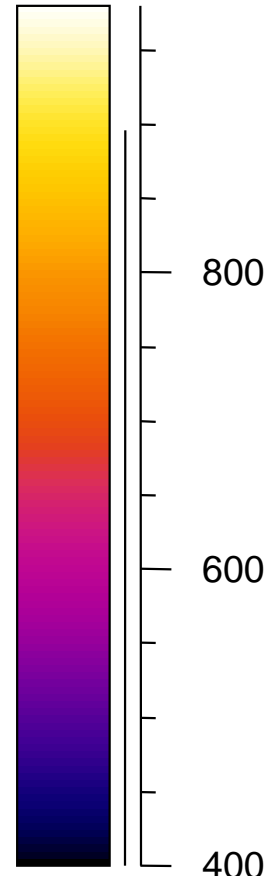
t = 50 min.

$\theta_{\text{con},\emptyset} = 730 \text{ }^\circ\text{C}$

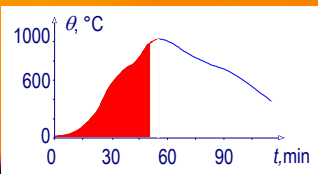


980,0°C

Buckling of the lower flange of the beam

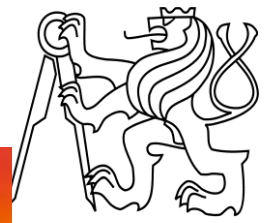


400,0°C



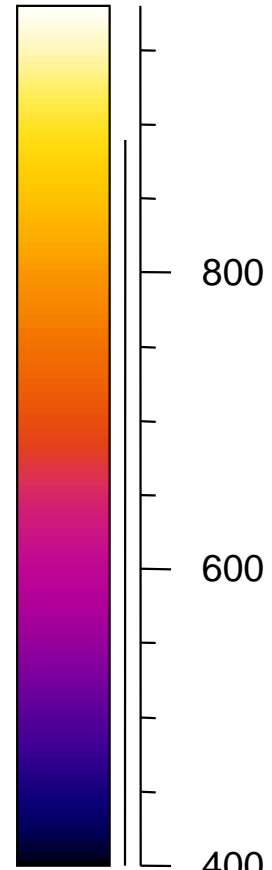
t = 52 min.

$\theta_{\text{con},\emptyset} = 775 \text{ } ^\circ\text{C}$

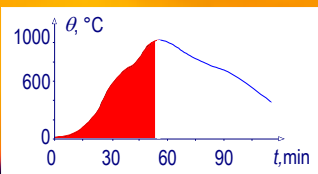


980,0°C

Buckling of the lower flange of the beam

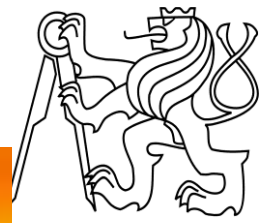


400,0°C

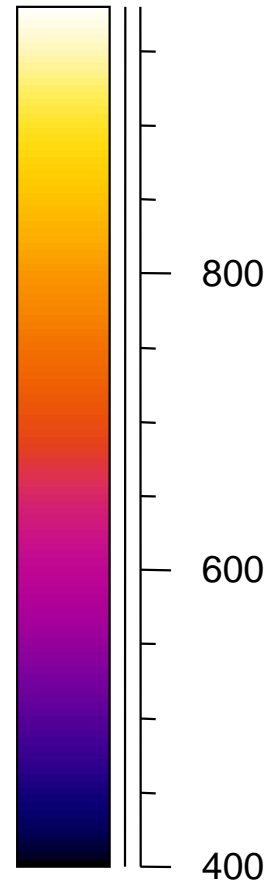


t = 54 min.

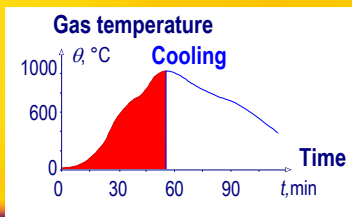
$\theta_{\text{con},\emptyset} = 810 \text{ }^\circ\text{C}$



980,0°C

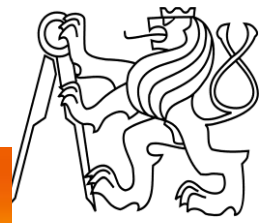


400,0°C



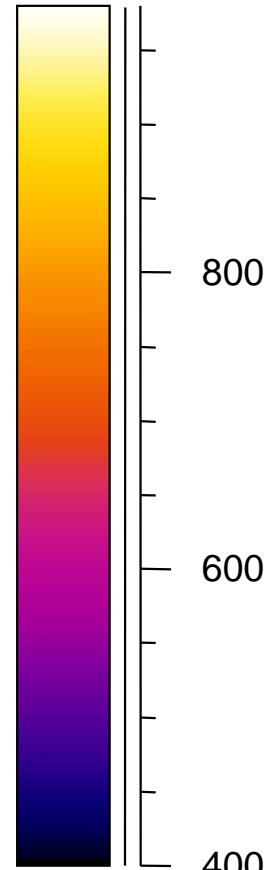
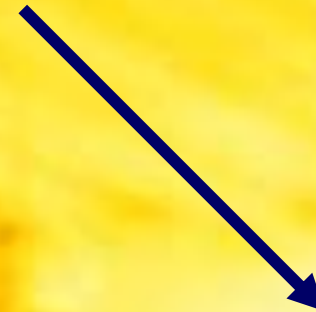
t = 56 min.

$\theta_{\text{con},\emptyset} = 835 \text{ }^\circ\text{C}$

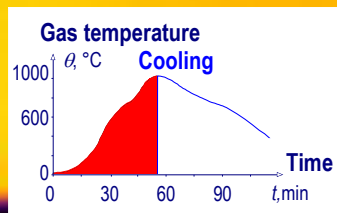


980,0°C

**Max temperature 1088 °C
at the lower flange in the
middle of the beam in 57 min**

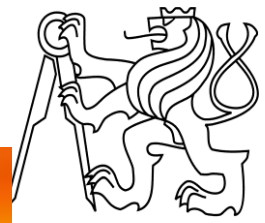


400,0°C



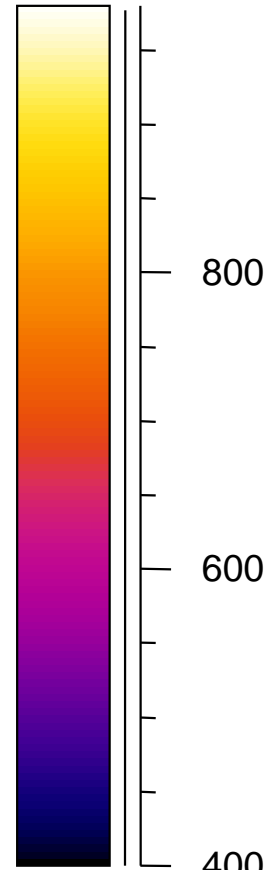
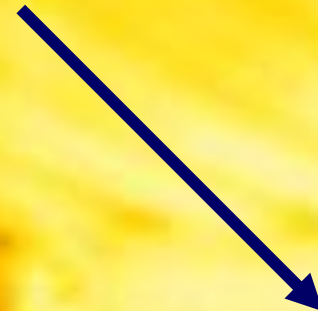
t = 58 min.

$\theta_{\text{con},\emptyset} = 855 \text{ }^\circ\text{C}$

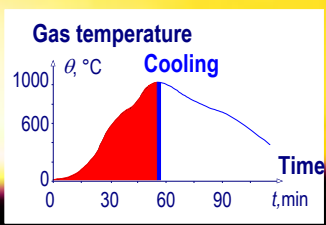


980,0°C

**Max temperature 1088 °C
at the lower flange in the
middle of the beam in 57 min**

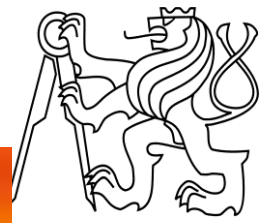


400,0°C

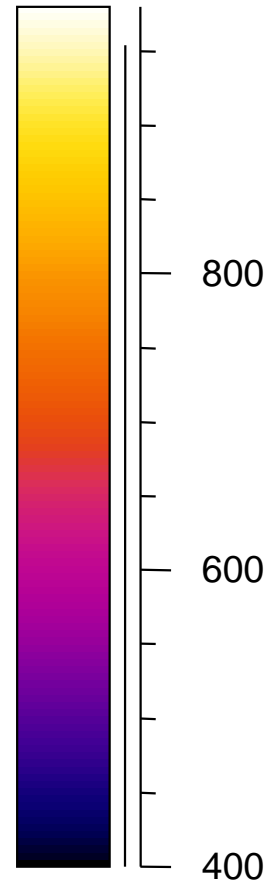


t = 60 min.

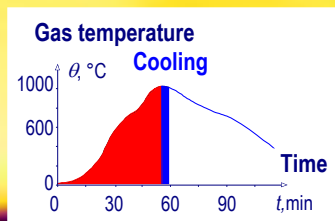
$\theta_{\text{con},\emptyset} = 880 \text{ }^\circ\text{C}$



980,0°C

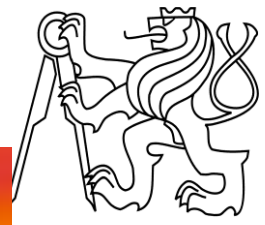


400,0°C



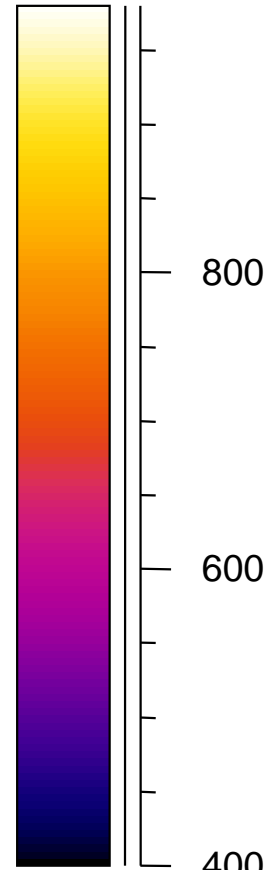
t = 62 min.

$\theta_{\text{con},\emptyset} = 900 \text{ }^\circ\text{C}$

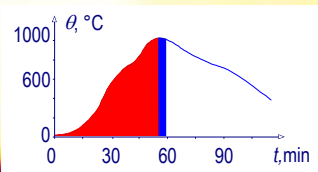


980,0°C

**Max temperature of the connection
908,3°C in 63 min**

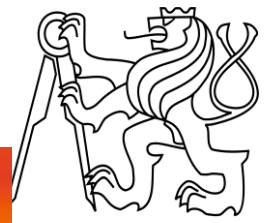


400,0°C



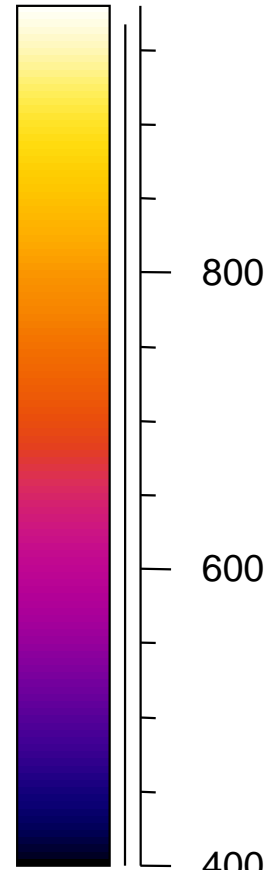
t = 64 min.

$\theta_{\text{con},\emptyset} = 885 \text{ }^{\circ}\text{C}$

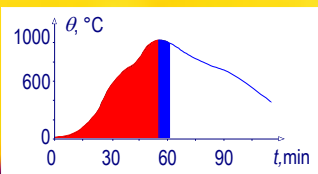


980,0°C

**Max temperature of the connection
908,3°C in 63 min**

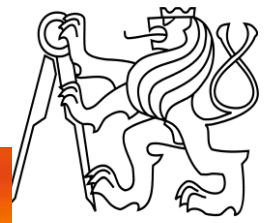


400,0°C

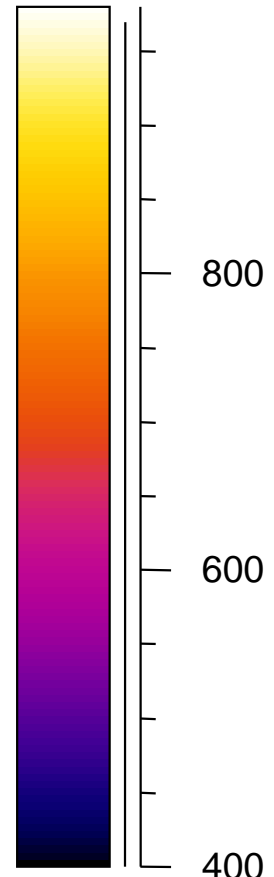


t = 66 min.

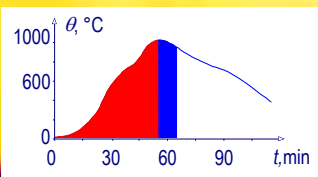
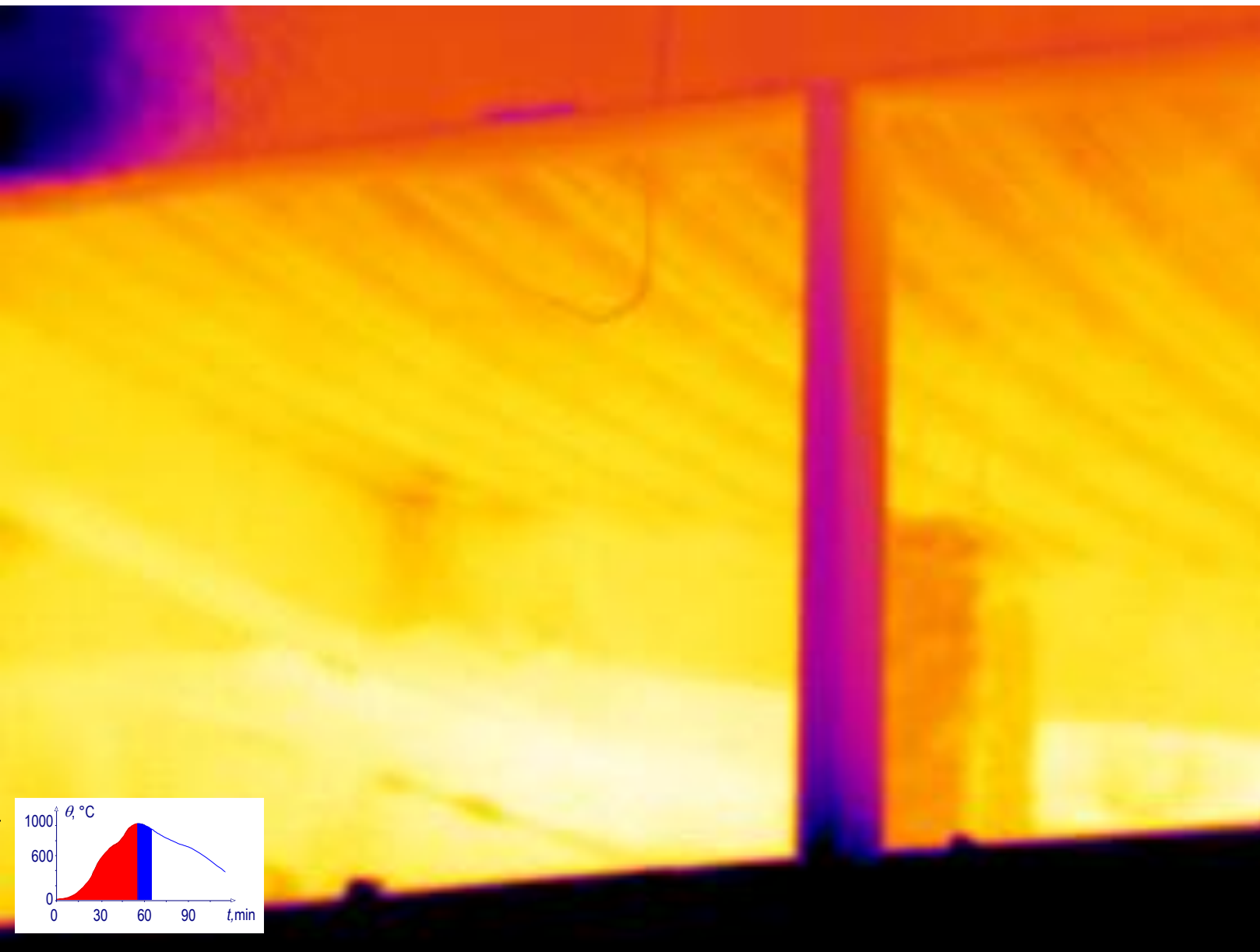
$\theta_{\text{con},\emptyset} = 860 \text{ }^\circ\text{C}$



980,0°C

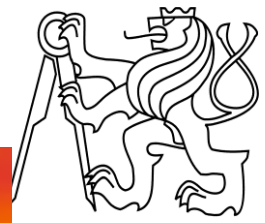


400,0°C

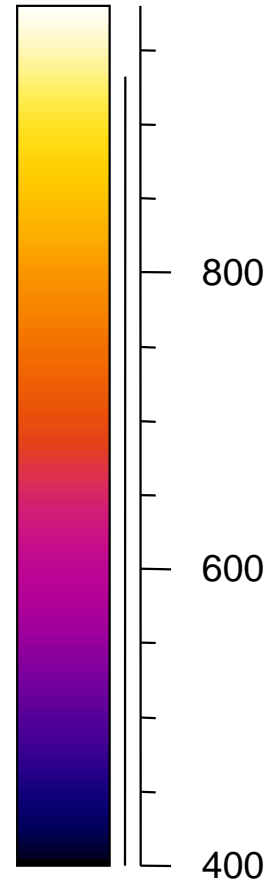


t = 68 min.

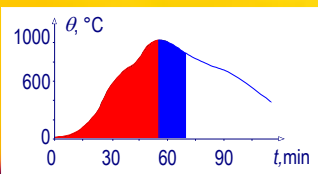
$\theta_{\text{con},\emptyset} = 840 \text{ }^\circ\text{C}$



980,0°C

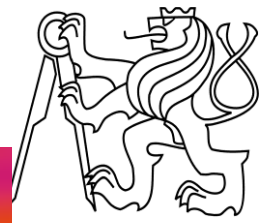


400,0°C

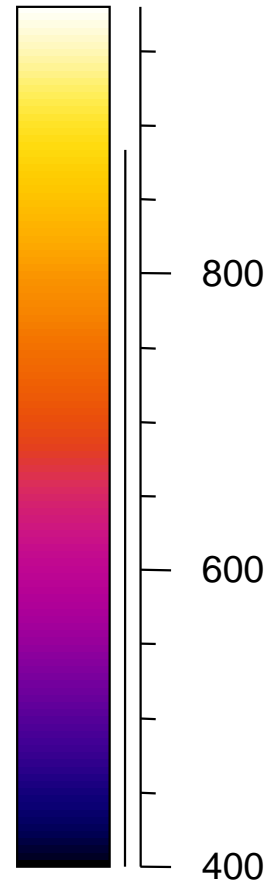


t = 70 min.

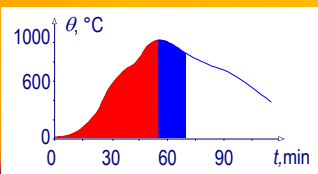
$\theta_{\text{con},\emptyset} = 820 \text{ }^\circ\text{C}$



980,0°C

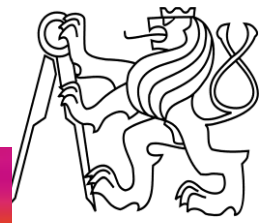


400,0°C



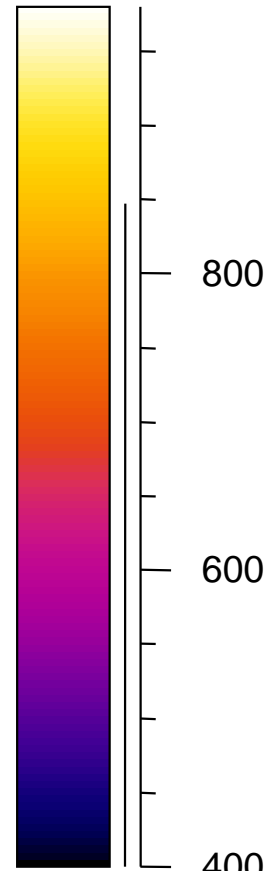
$$t = t_0 + 1 \text{ h } 12'$$

$$T_{\text{con},\emptyset} = 800 \text{ }^\circ\text{C}$$

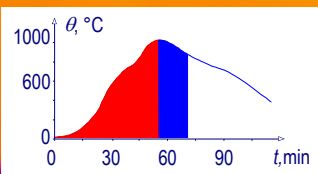


980,0°C

Temperature of the connection is higher than the beam. But the temperature is lower than max. temp. of the beam.

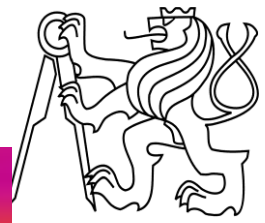


400,0°C

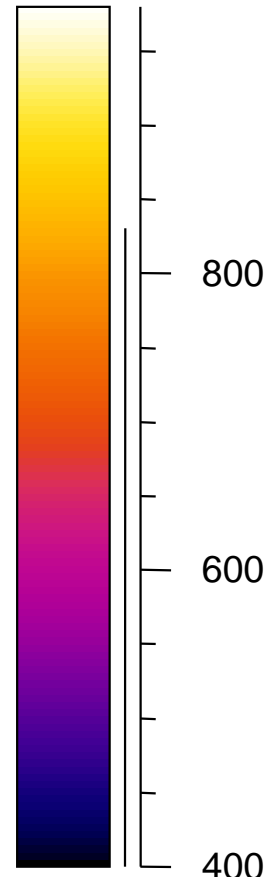


t = 74 min.

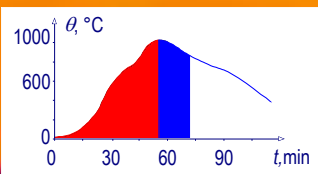
$\theta_{\text{con},\emptyset} = 790 \text{ }^\circ\text{C}$



980,0°C

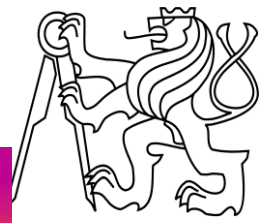


400,0°C

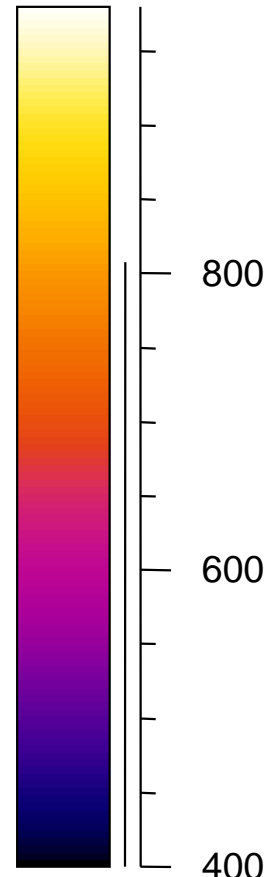


t = 76 min.

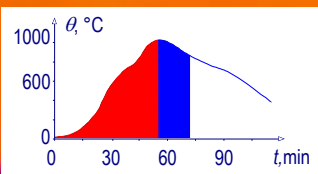
$\theta_{\text{con},\emptyset} = 770 \text{ }^{\circ}\text{C}$



980,0°C

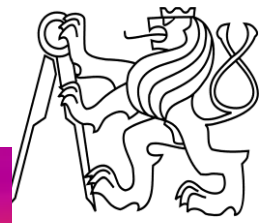


400,0°C

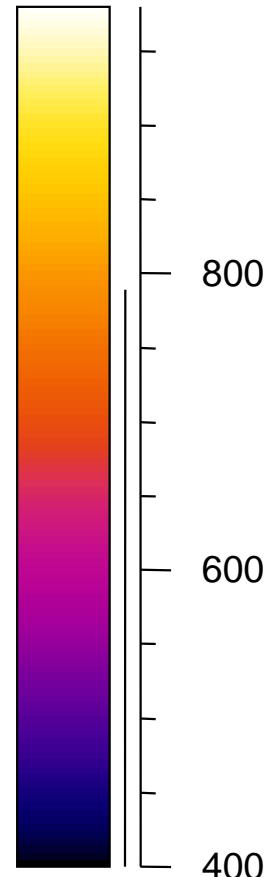


t = 78 min.

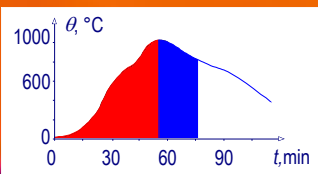
$\theta_{\text{con},\emptyset} = 775 \text{ }^{\circ}\text{C}$



980,0°C

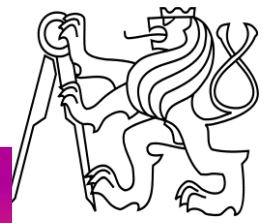


400,0°C

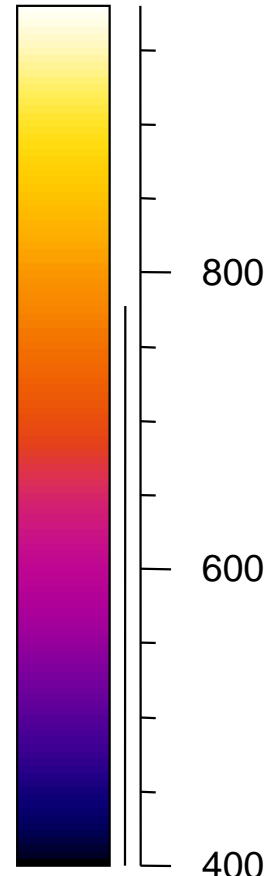


t = 80 min.

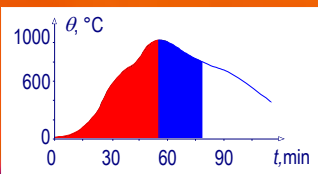
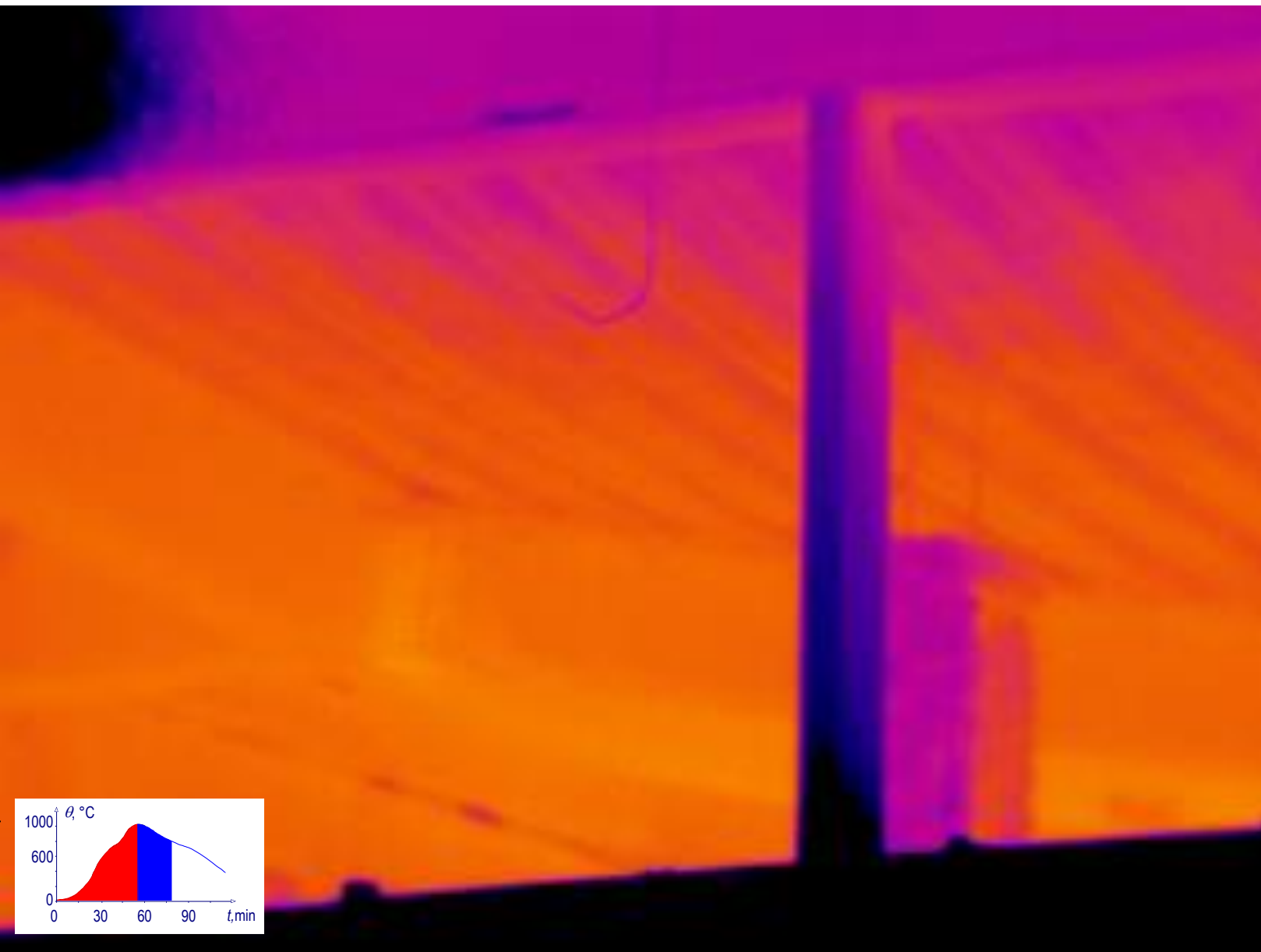
$\theta_{\text{con},\emptyset} = 745 \text{ }^\circ\text{C}$



980,0°C

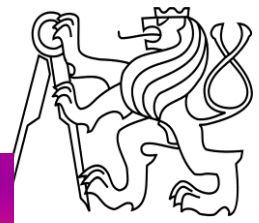


400,0°C

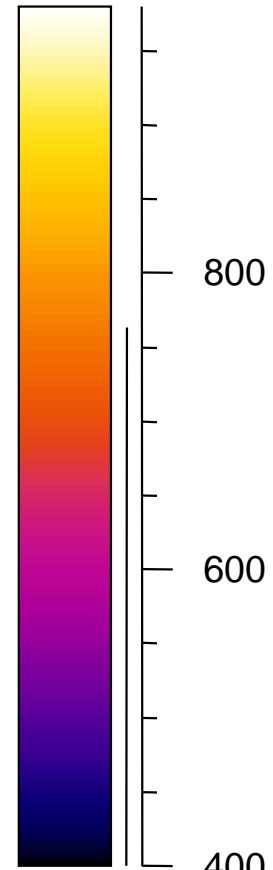


t = 82 min.

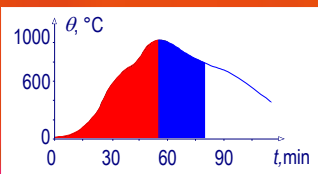
$\theta_{\text{con},\emptyset} = 740 \text{ }^\circ\text{C}$



980,0°C

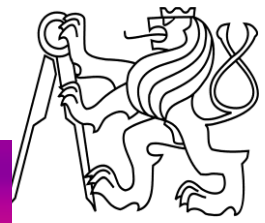


400,0°C

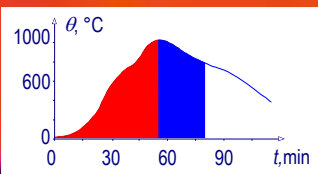
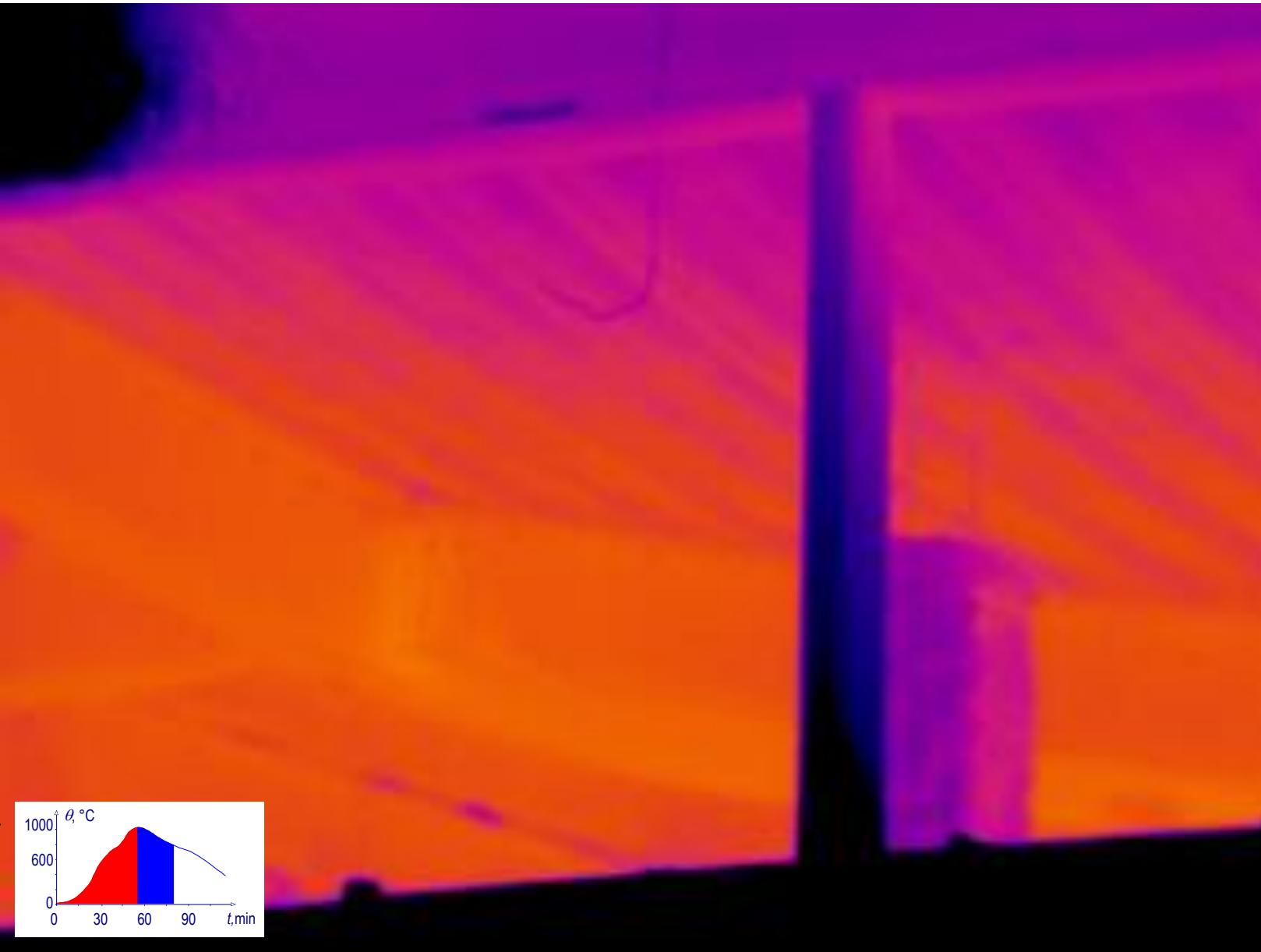
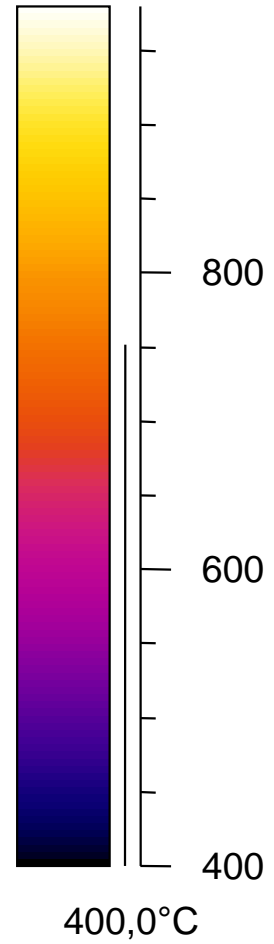


t = 84 min.

$\theta_{\text{con},\emptyset} = 730 \text{ }^{\circ}\text{C}$

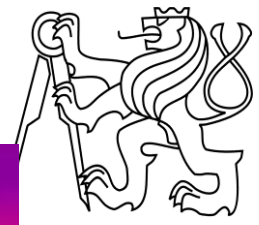


980,0°C

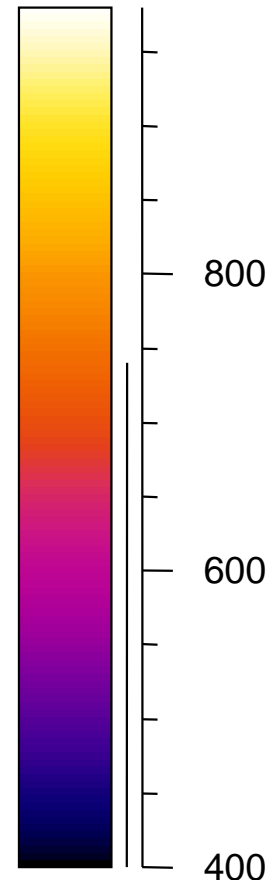


t = 76 min.

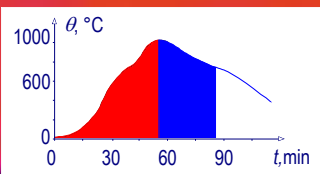
$\theta_{\text{con},\emptyset} = 720 \text{ }^{\circ}\text{C}$



980,0°C

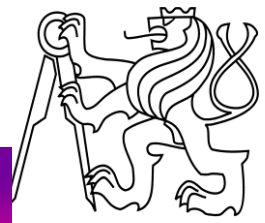


400,0°C

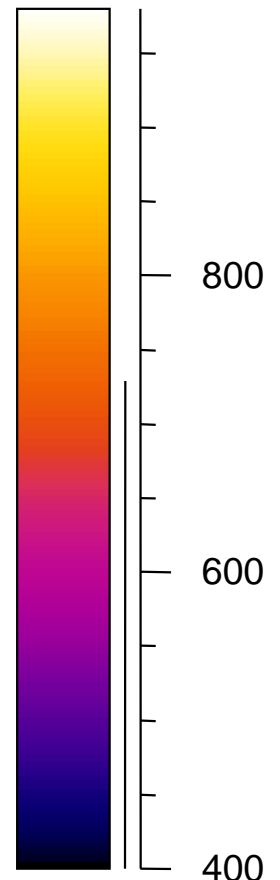


t = 78 min.

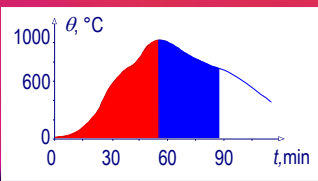
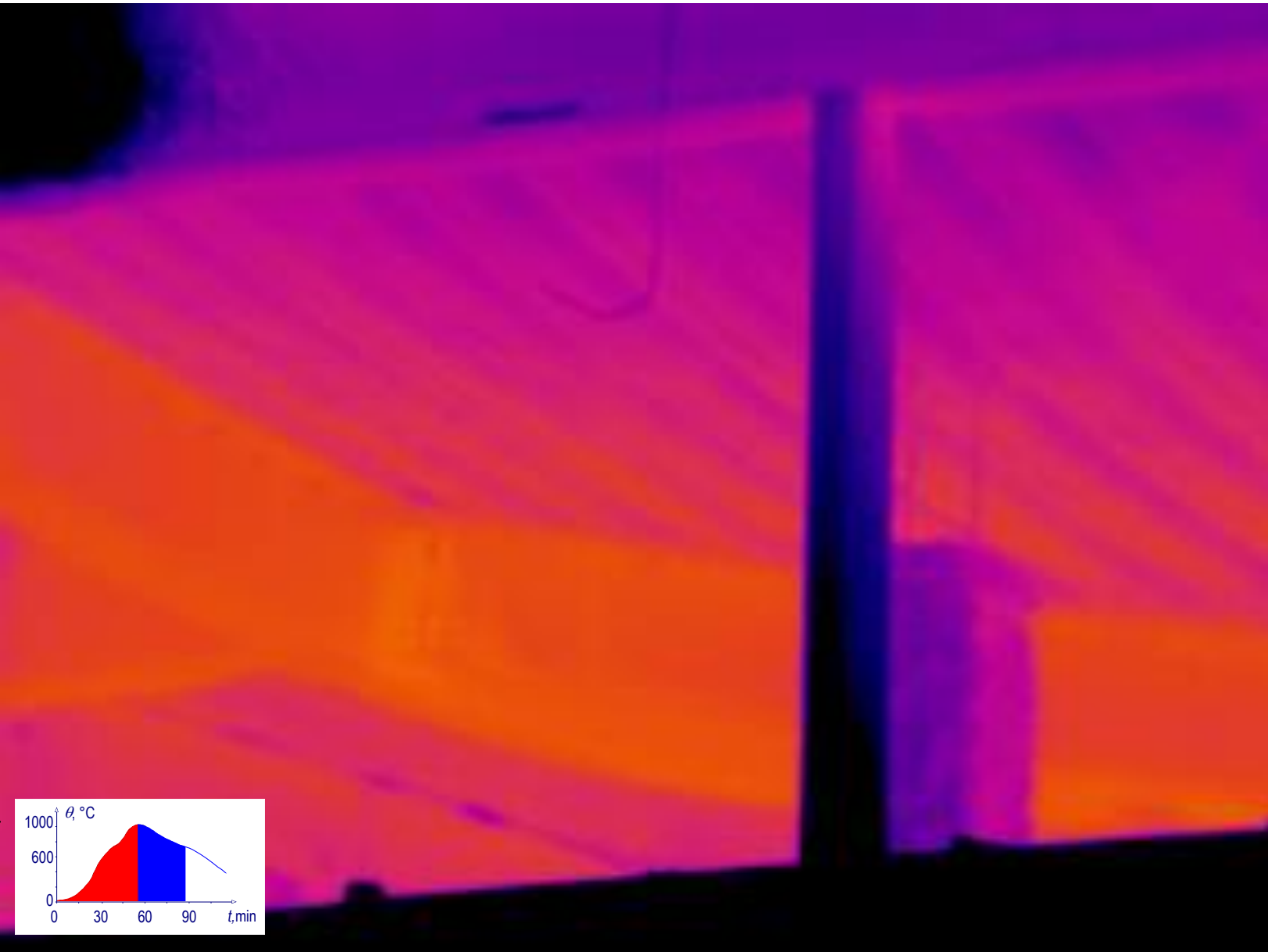
$\theta_{\text{con},\emptyset} = 710 \text{ }^{\circ}\text{C}$



980,0°C

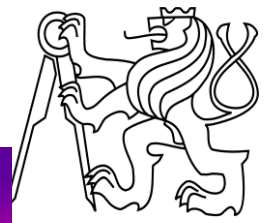


400,0°C

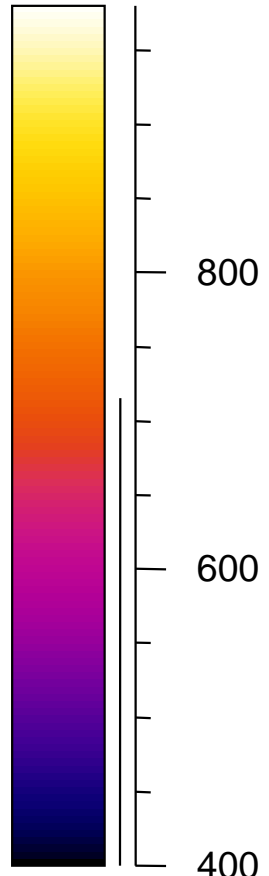


t = 90 min.

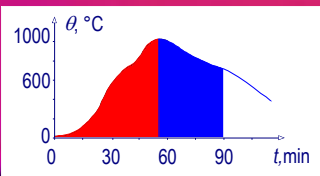
$\theta_{\text{con},\emptyset} = 690 \text{ }^\circ\text{C}$



980,0°C

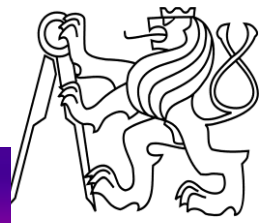


400,0°C

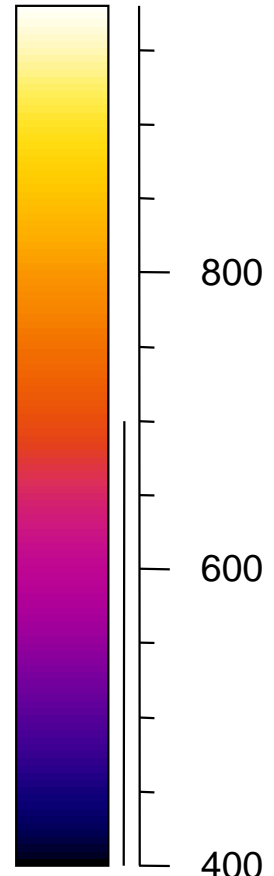


t = 92 min.

$\theta_{\text{con},\emptyset} = 680 \text{ }^{\circ}\text{C}$



980,0°C

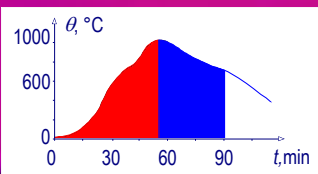
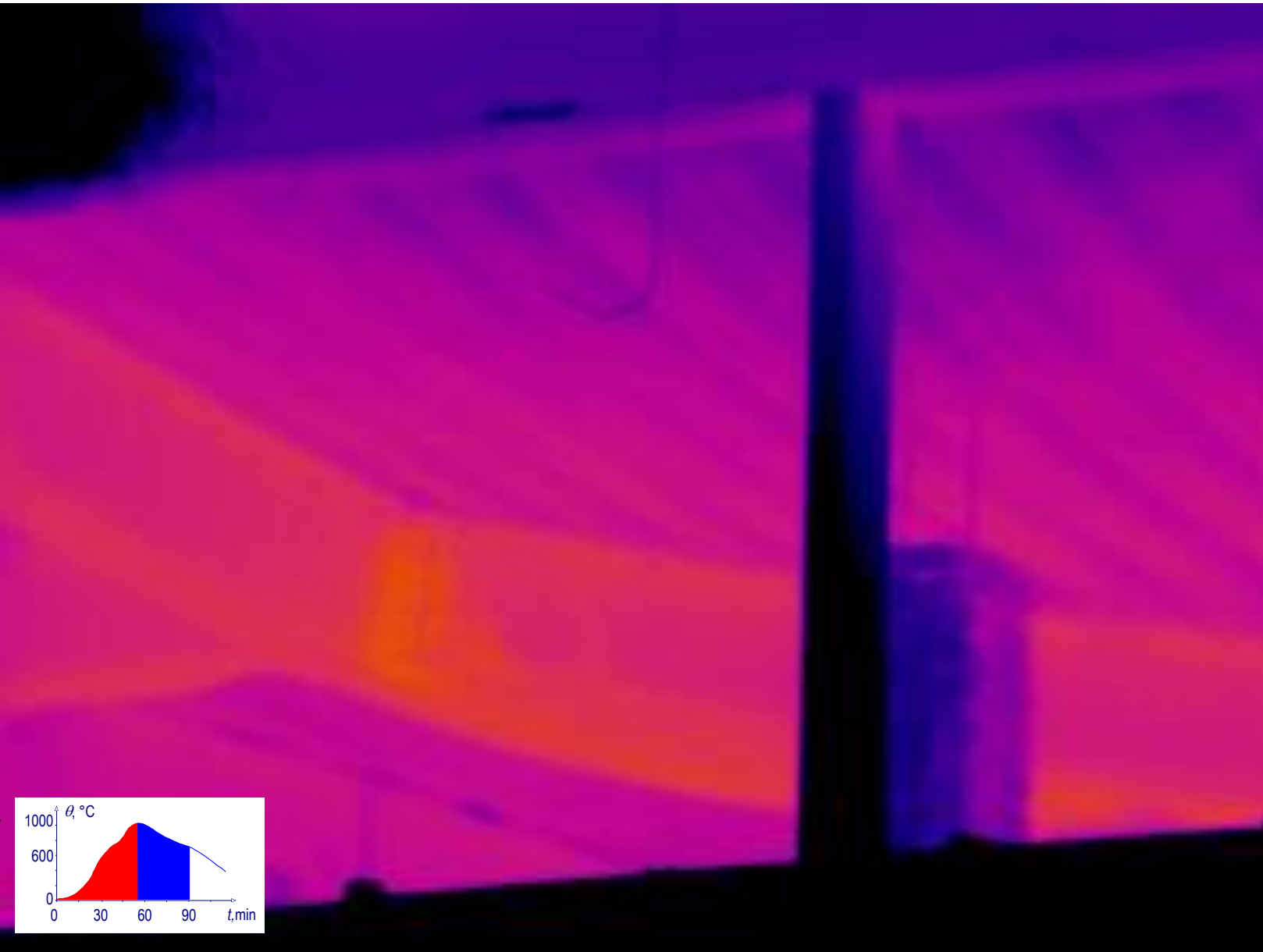


800

600

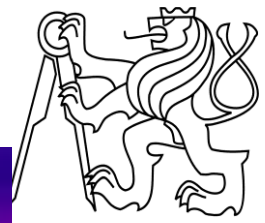
400

400,0°C

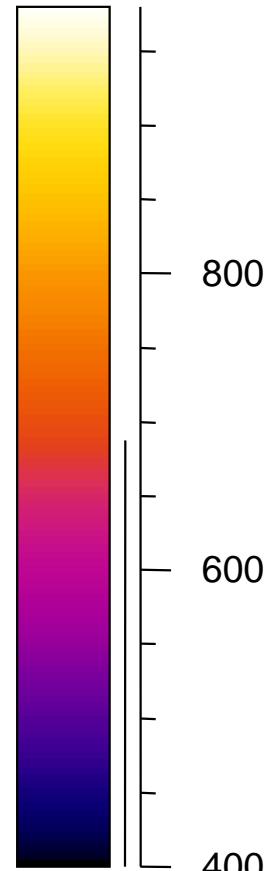


t = 94 min.

$\theta_{\text{con},\emptyset} = 670 \text{ }^\circ\text{C}$



980,0°C

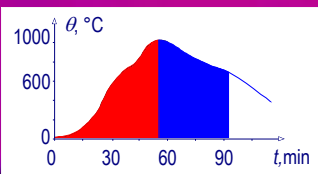
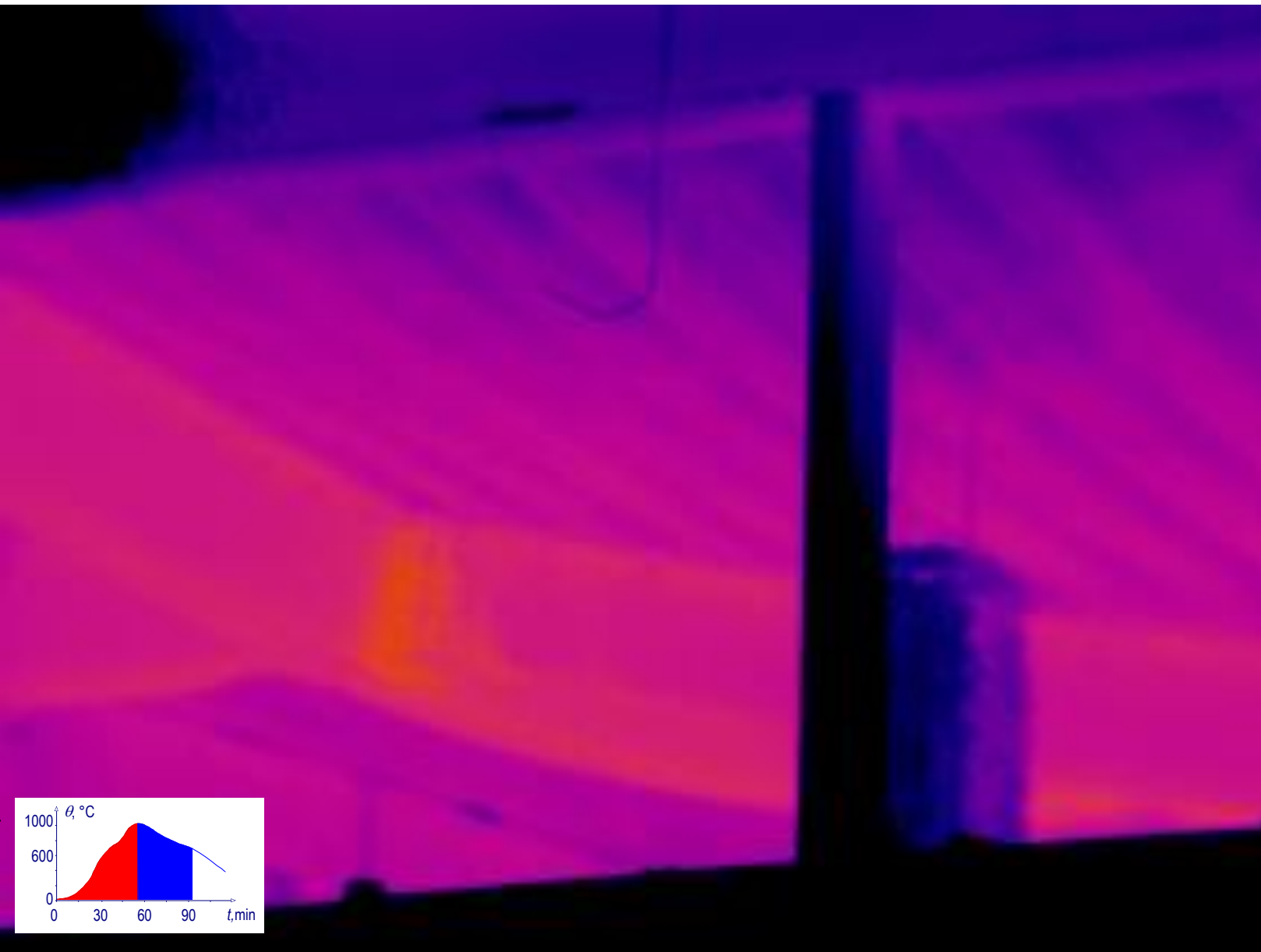


800

600

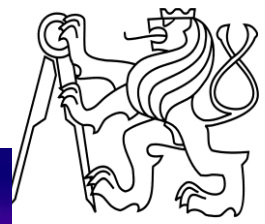
400

400,0°C

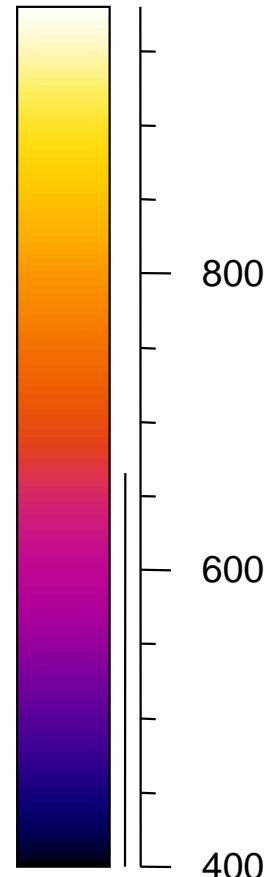


t = 96 min.

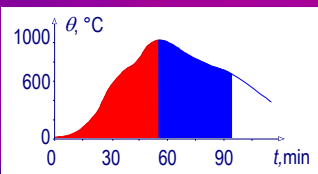
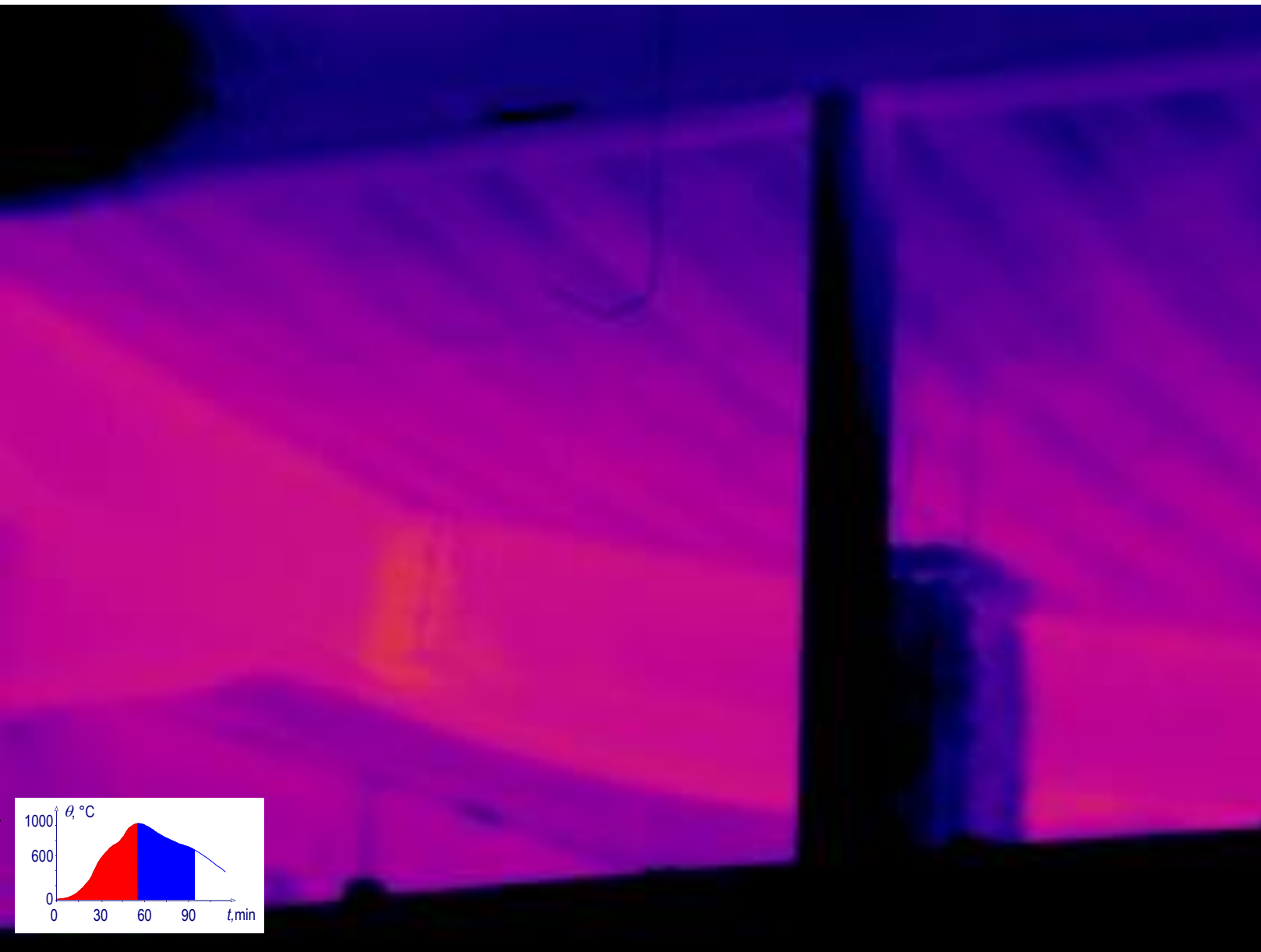
$\theta_{\text{con},\emptyset} = 650 \text{ }^{\circ}\text{C}$



980,0°C

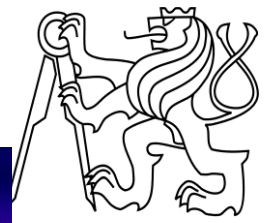


400,0°C

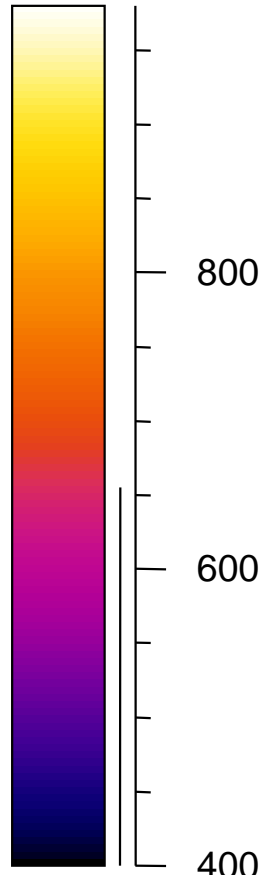


t = 98 min.

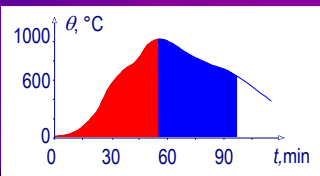
$\theta_{\text{con},\emptyset} = 640 \text{ }^{\circ}\text{C}$



980,0°C

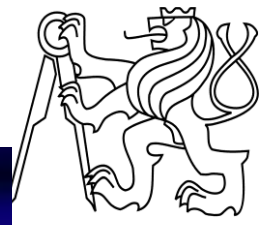


400,0°C

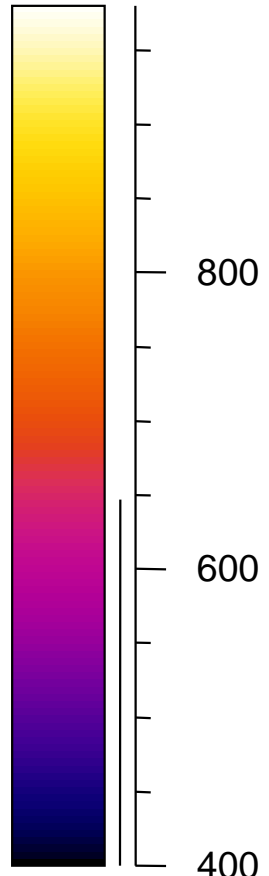


t = 100 min.

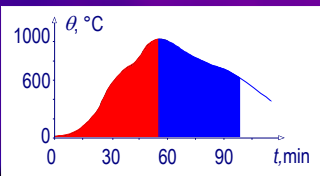
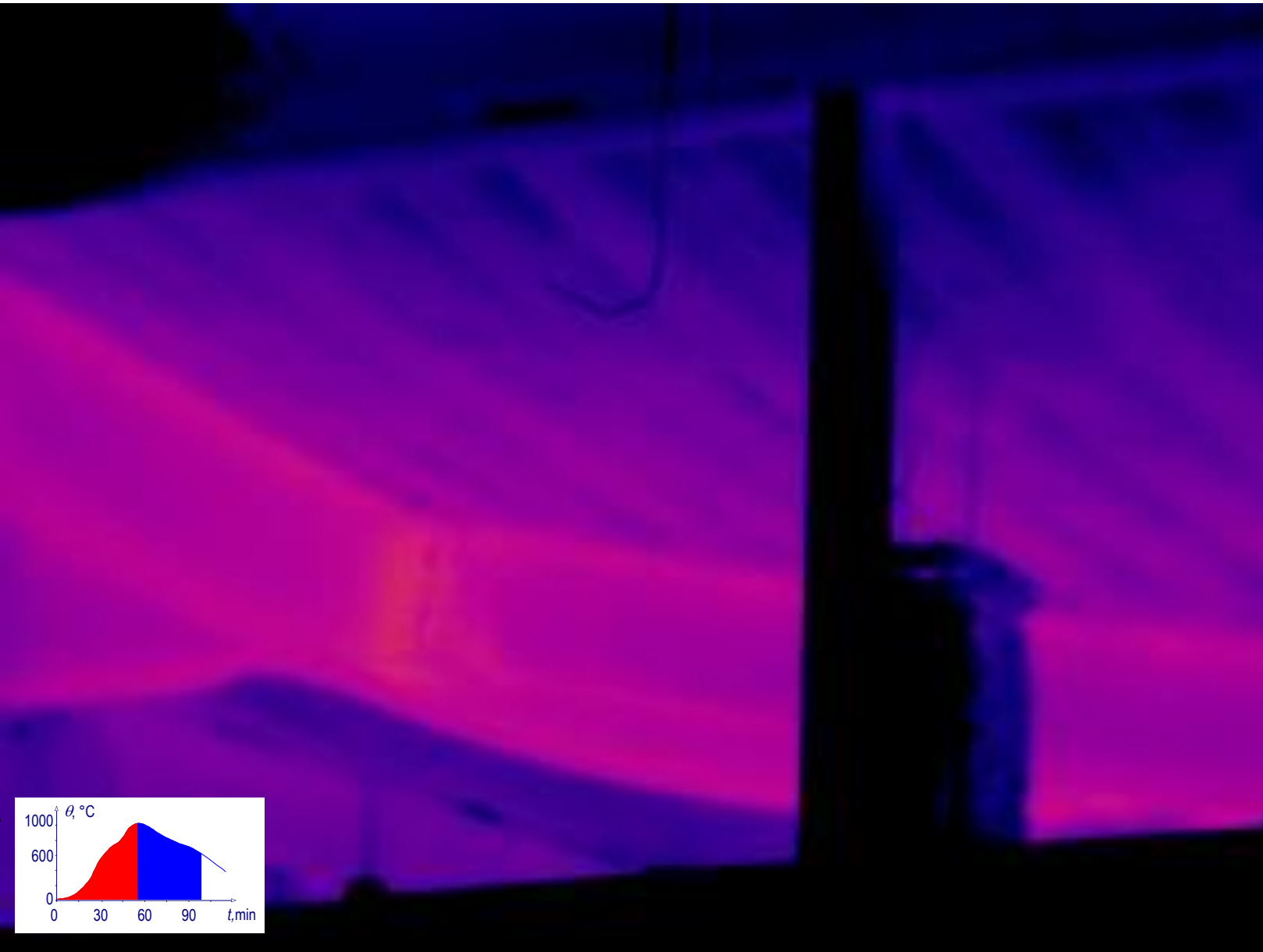
$\theta_{\text{con},\emptyset} = 635 \text{ }^\circ\text{C}$



980,0°C

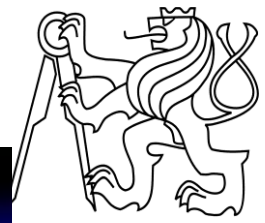


400,0°C

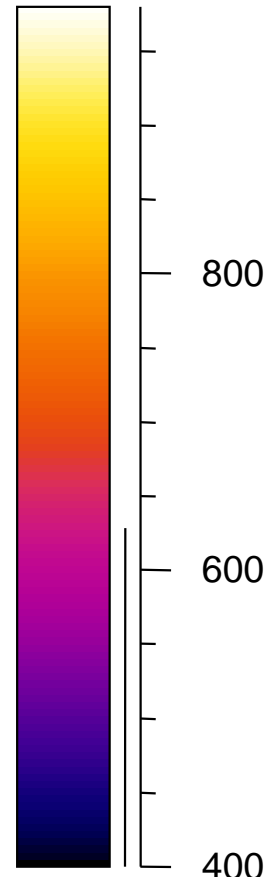


t = 102 min.

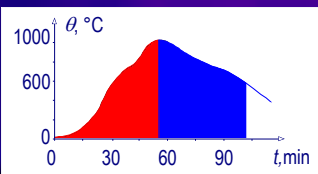
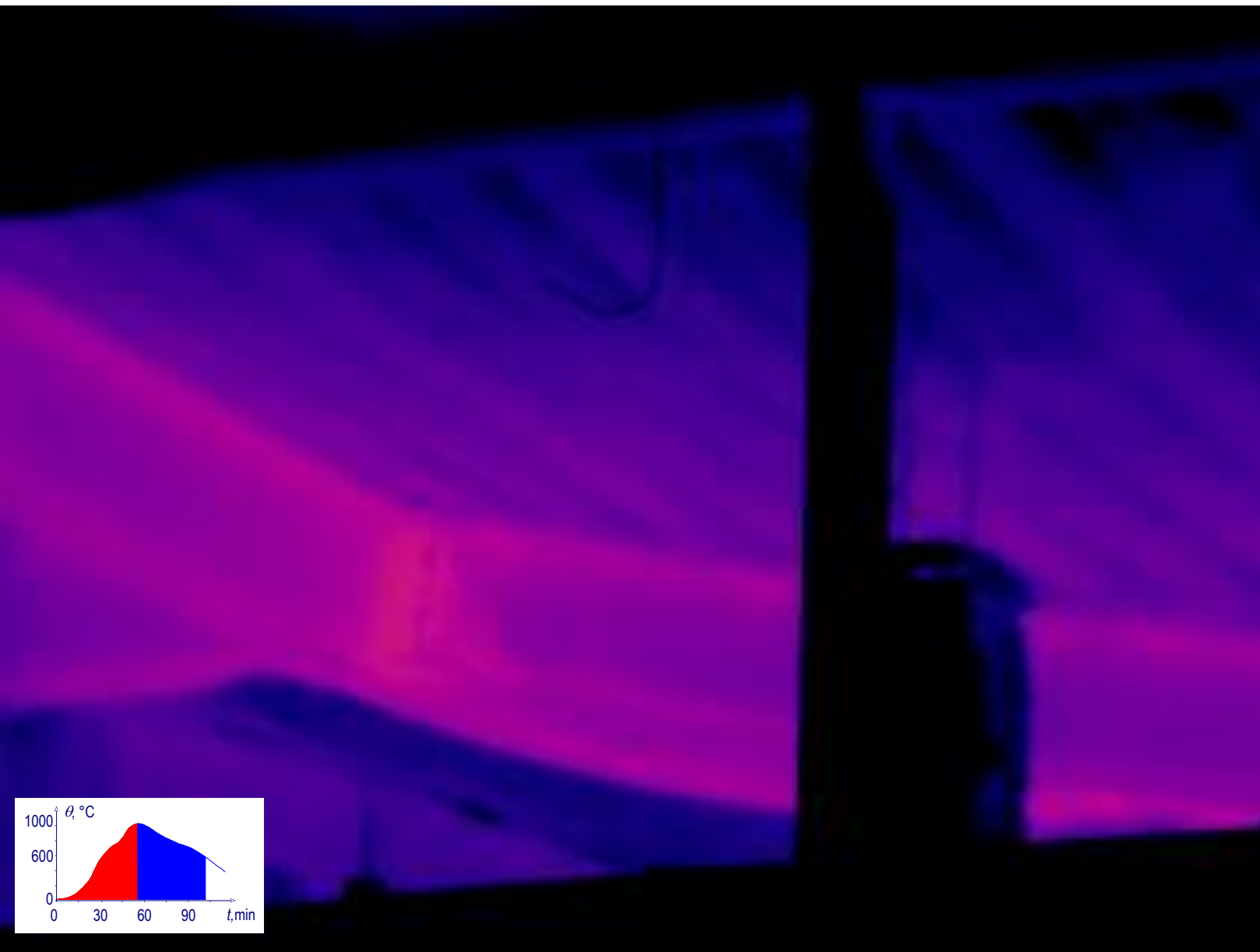
$\theta_{\text{con},\emptyset} = 620 \text{ }^{\circ}\text{C}$



980,0°C

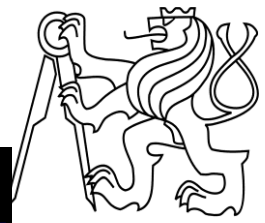


400,0°C

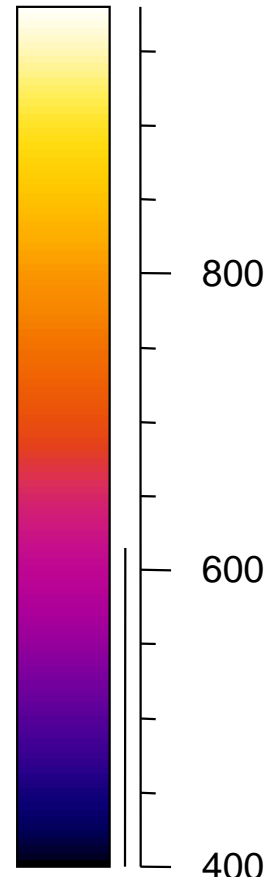


$t = 104 \text{ min.}$

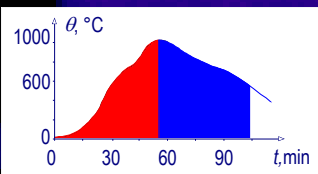
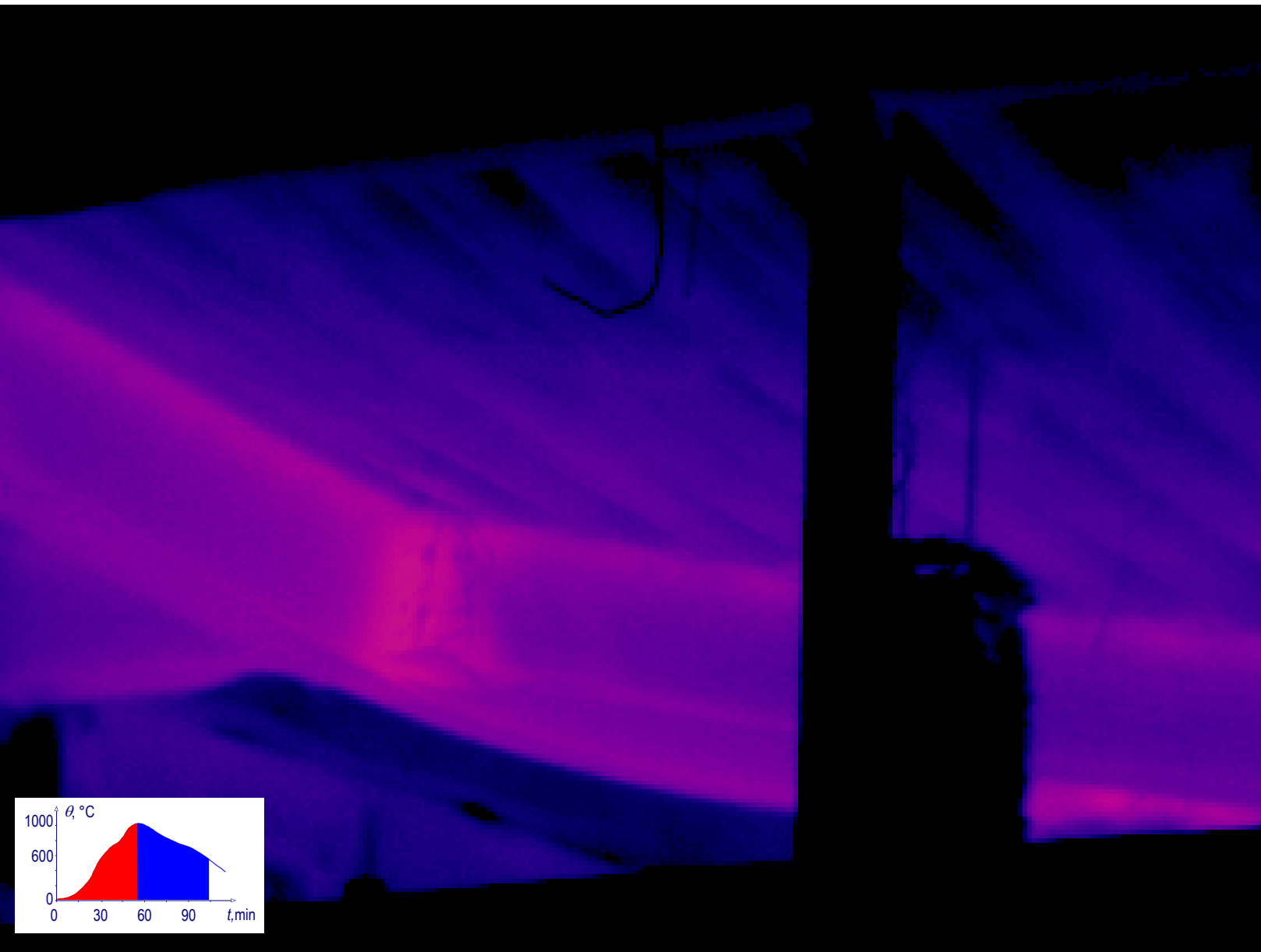
$\theta_{\text{con},\emptyset} = 600 \text{ }^\circ\text{C}$



980,0°C

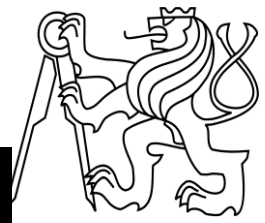


400,0°C

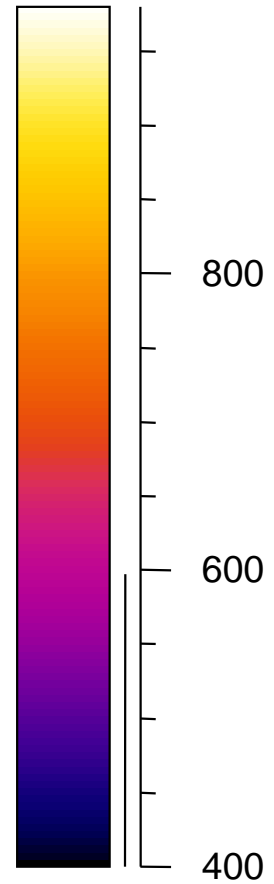


t = 106 min.

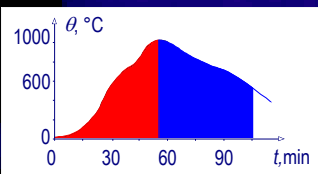
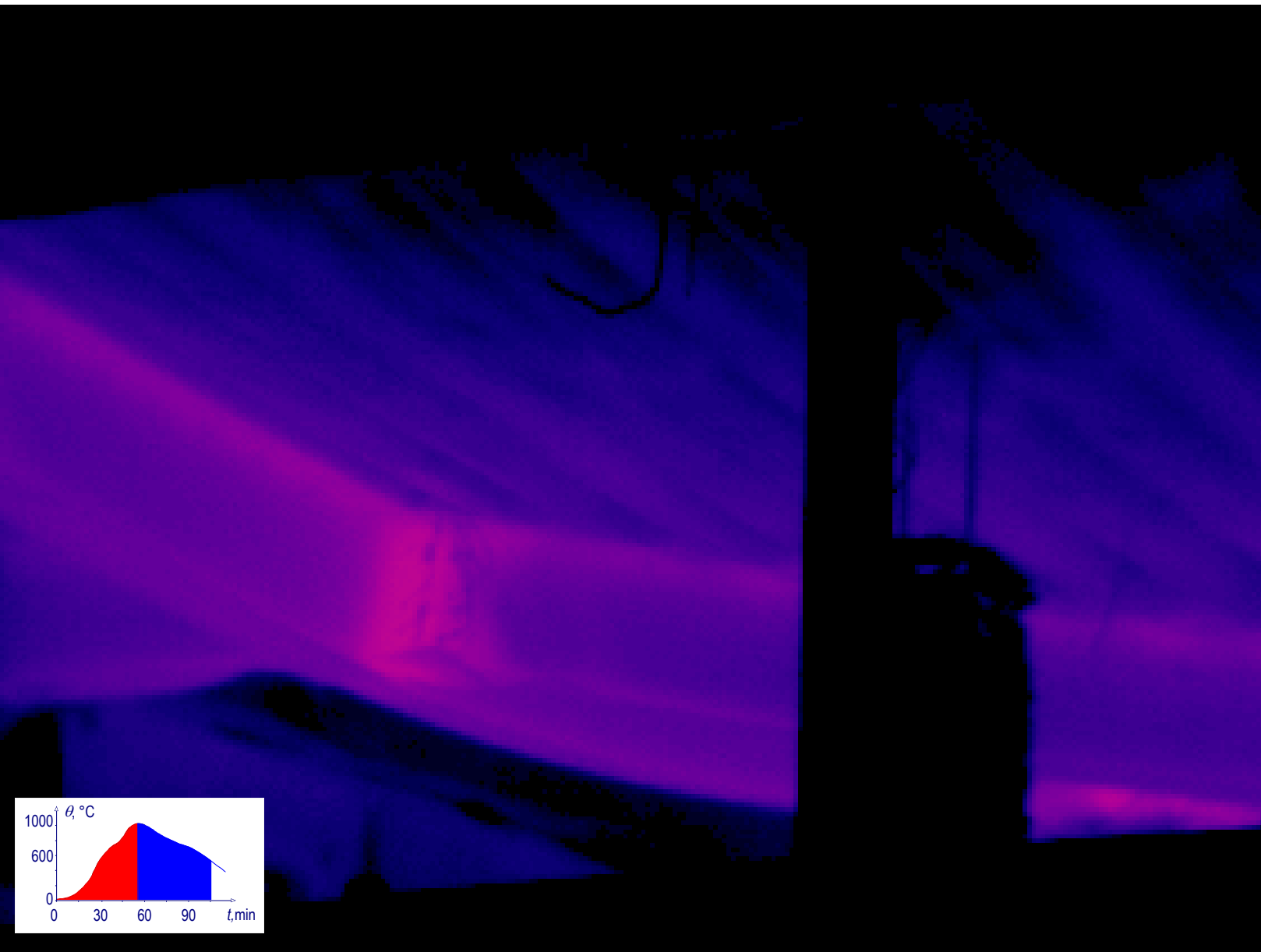
$\theta_{\text{con},\emptyset} = 585 \text{ }^\circ\text{C}$



980,0°C

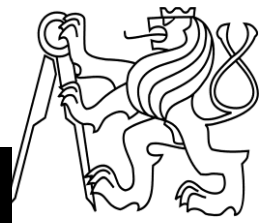


400,0°C

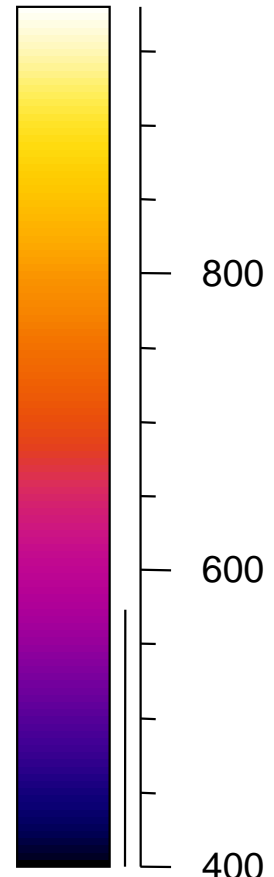


t = 108 min.

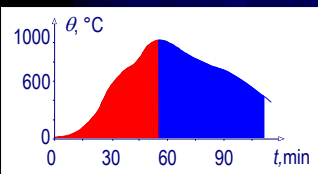
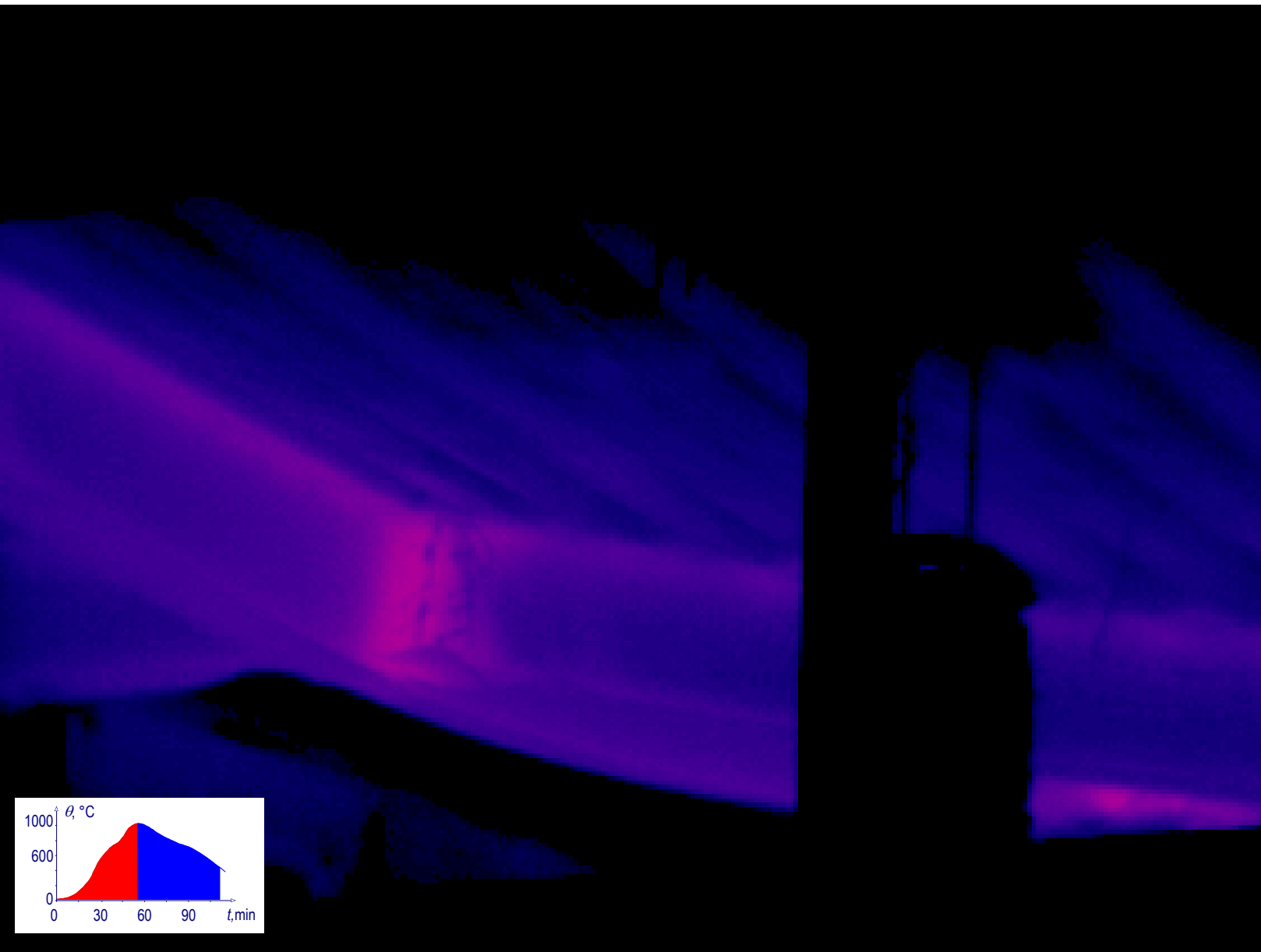
$\theta_{\text{con},\emptyset} = 560 \text{ }^\circ\text{C}$



980,0°C

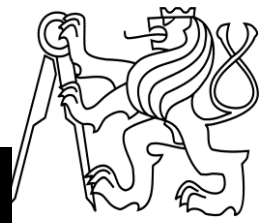


400,0°C

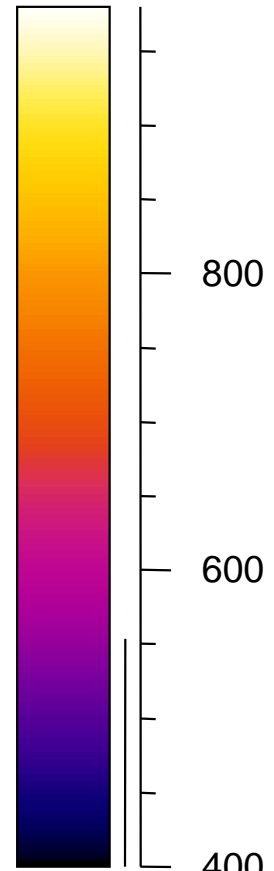


t = 110 min.

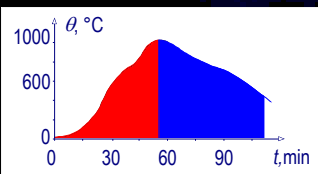
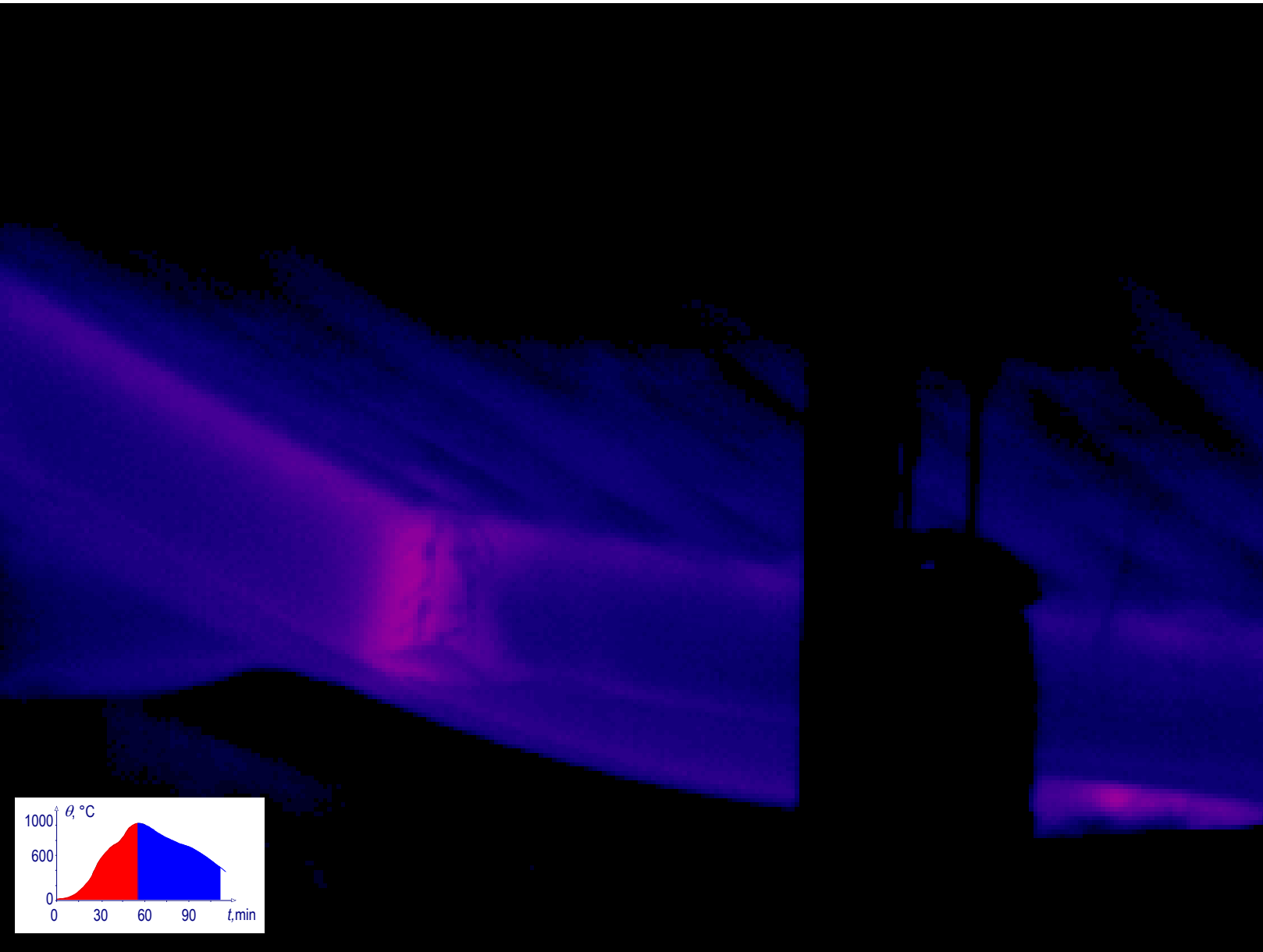
$\theta_{\text{con},\emptyset} = 540 \text{ }^{\circ}\text{C}$



980,0°C

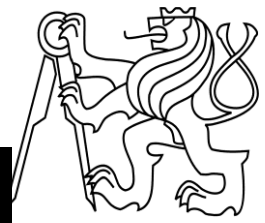


400,0°C

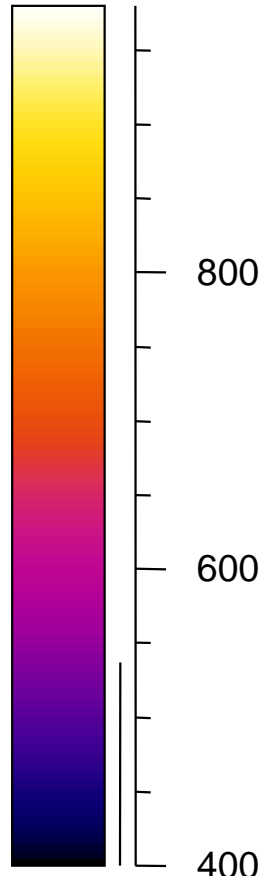


t = 112 min.

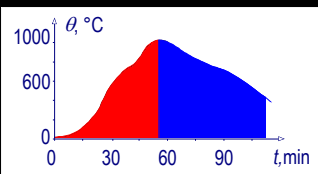
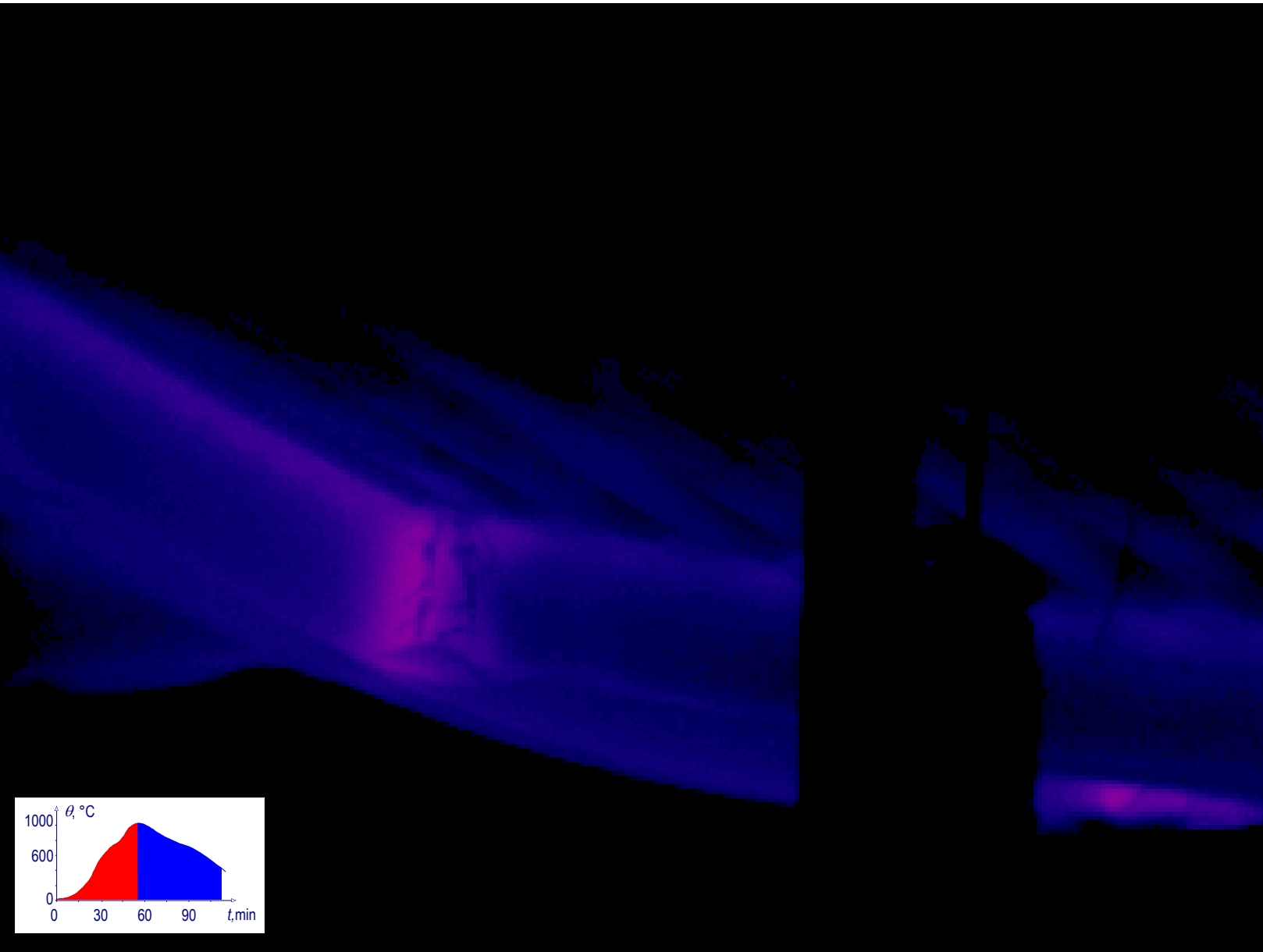
$\theta_{\text{con},\emptyset} = 520 \text{ }^\circ\text{C}$



980,0°C

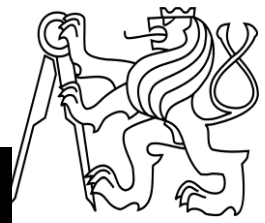


400,0°C

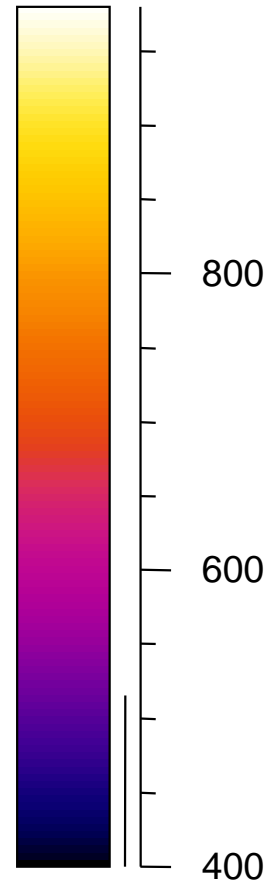


t = 114 min.

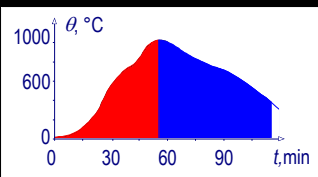
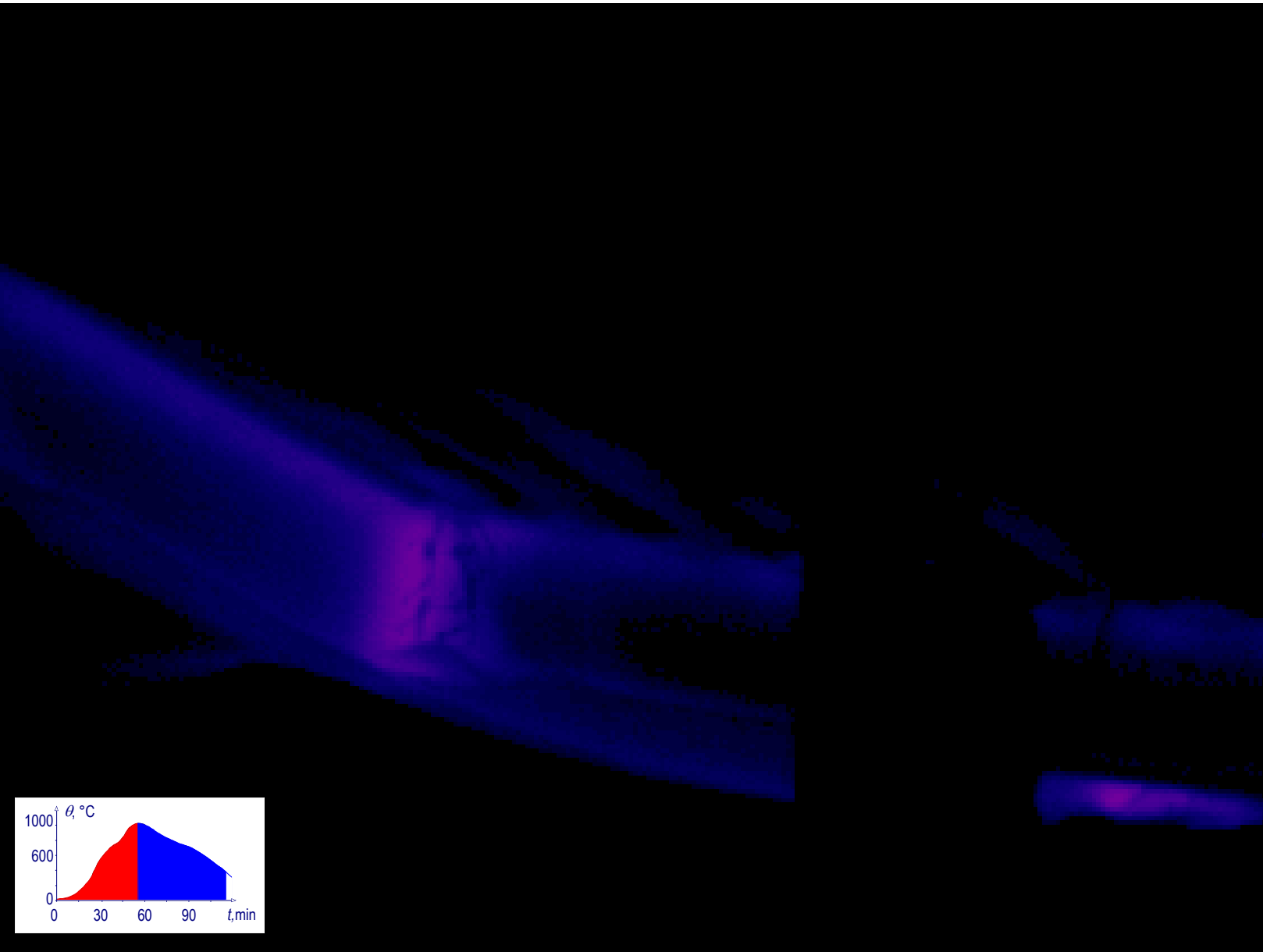
$\theta_{\text{con},\emptyset} = 505 \text{ }^{\circ}\text{C}$



980,0°C

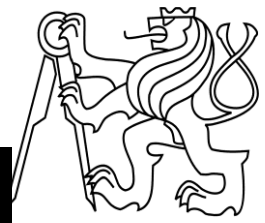


400,0°C



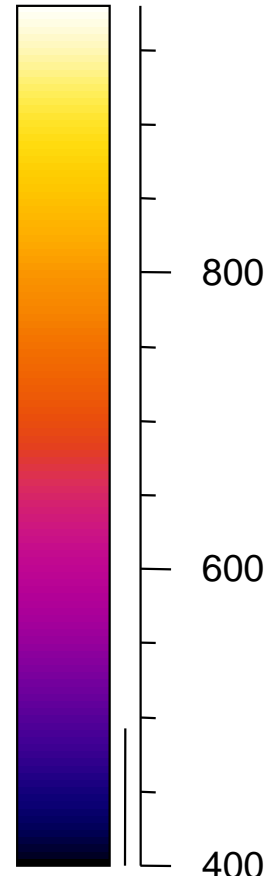
$t = 116 \text{ min.}$

$\theta_{\text{con},\emptyset} = 585 \text{ }^\circ\text{C}$

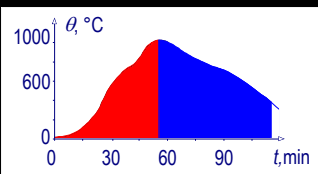


After 2 hours temperature of the structure
below 400°C

$980,0^\circ\text{C}$

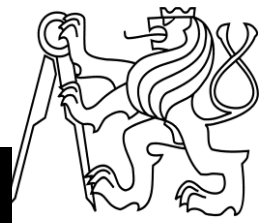


$400,0^\circ\text{C}$

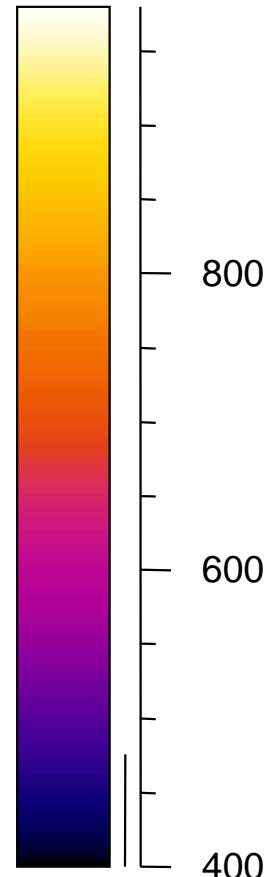


t = 118 min.

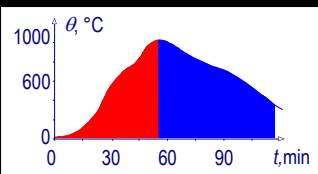
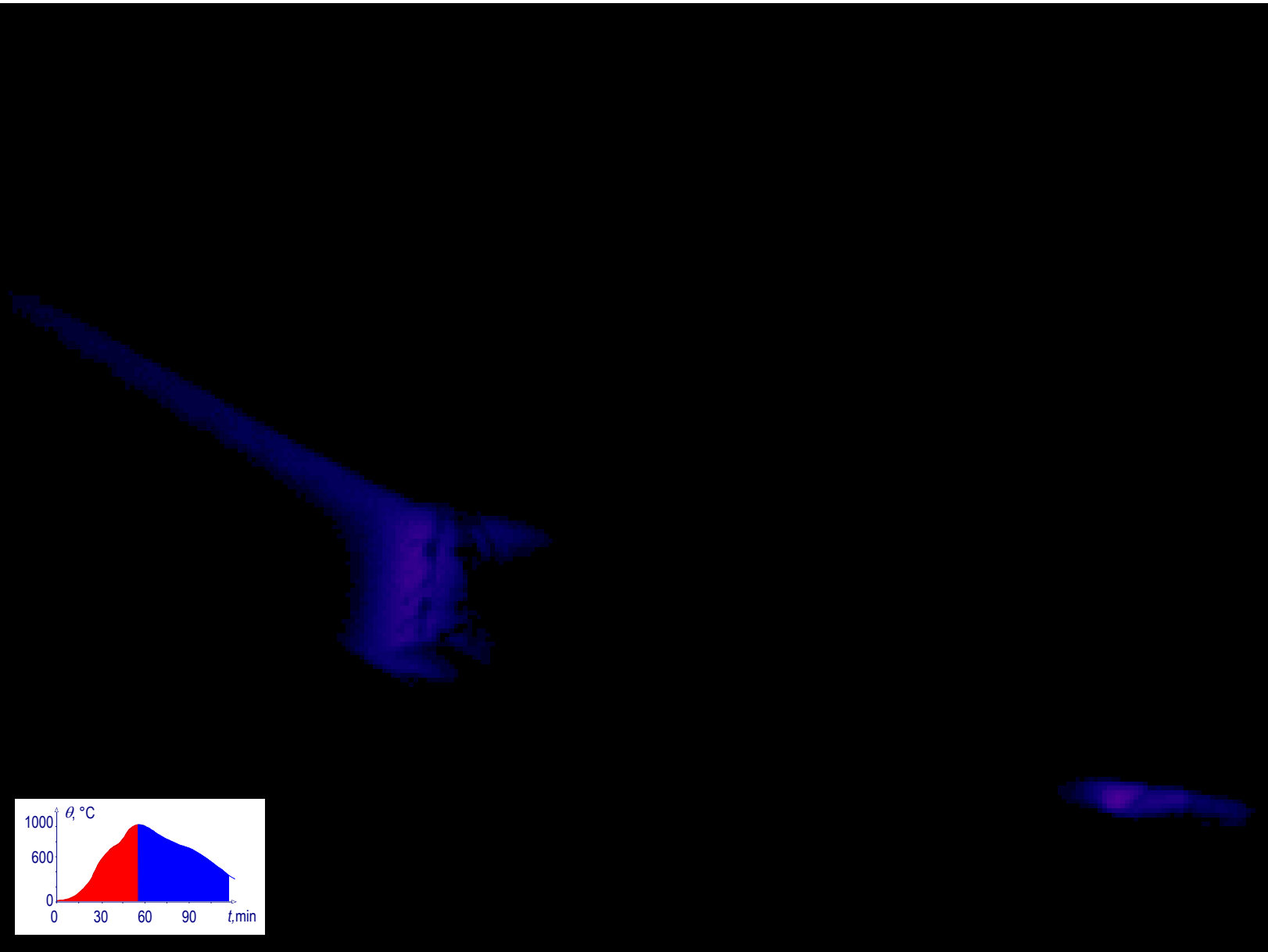
$\theta_{\text{con},\emptyset} = 470 \text{ }^\circ\text{C}$



980,0°C

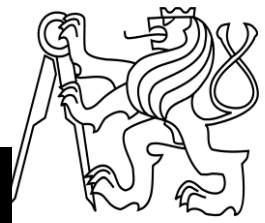


400,0°C

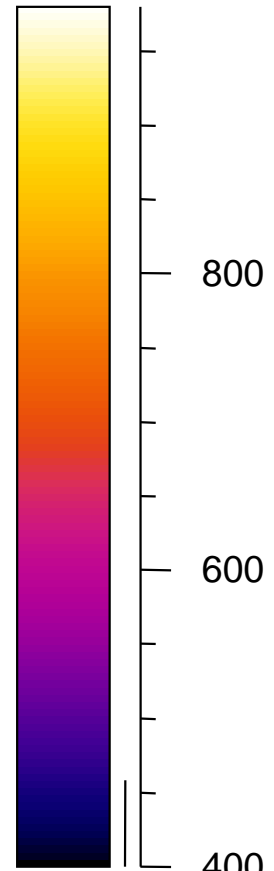


t = 120 min.

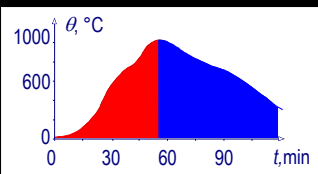
$\theta_{\text{con},\emptyset} = 450 \text{ }^\circ\text{C}$



980,0°C

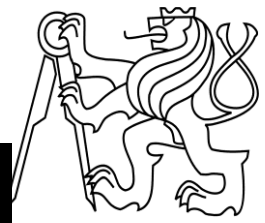


400,0°C

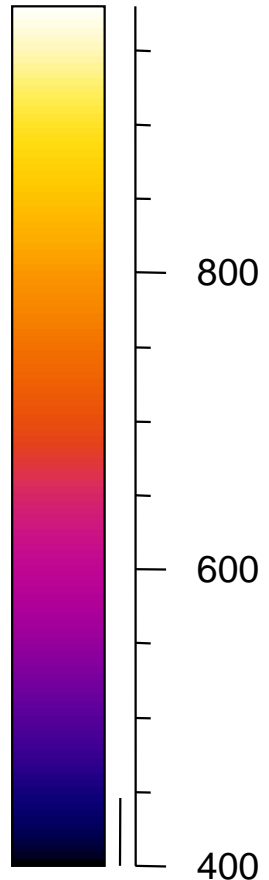


t = 122 min.

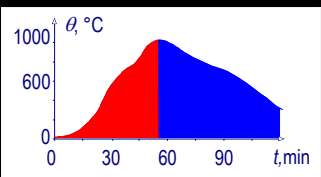
$\theta_{\text{con},\emptyset} = 435 \text{ }^\circ\text{C}$

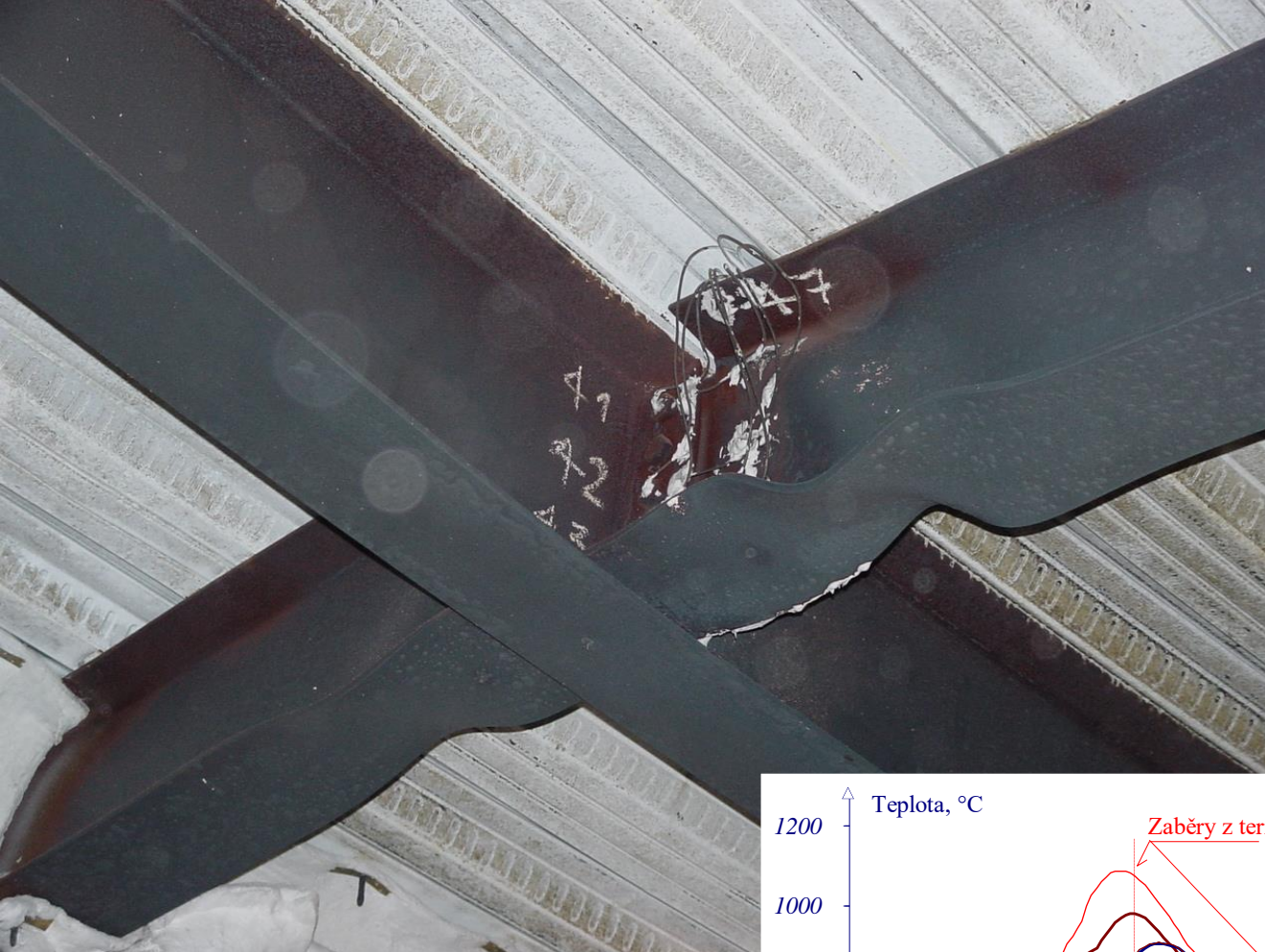


980,0°C

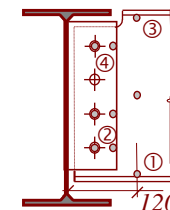
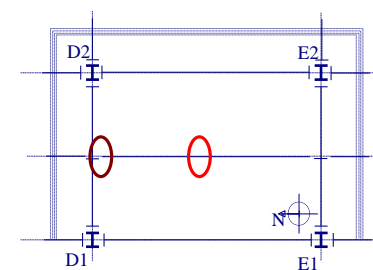
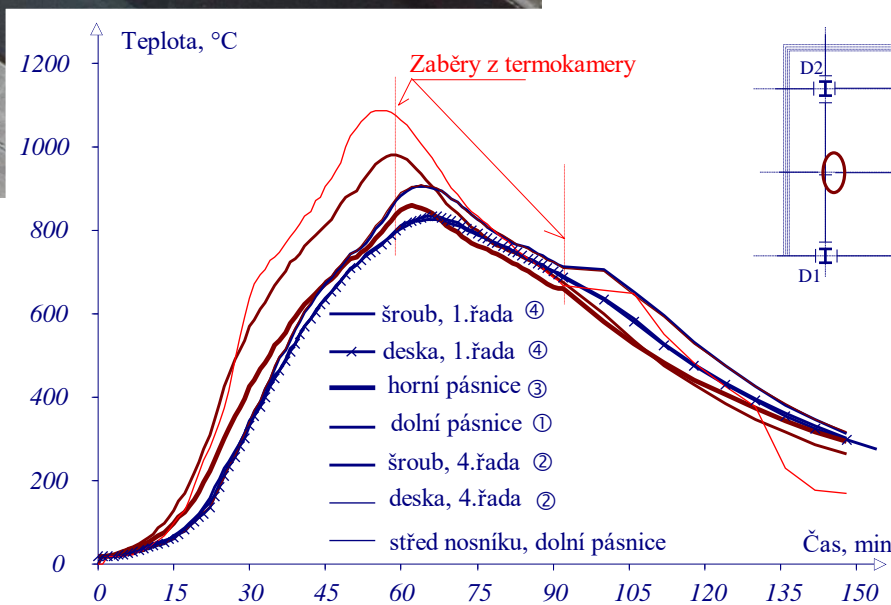


400,0°C





Connection after the test

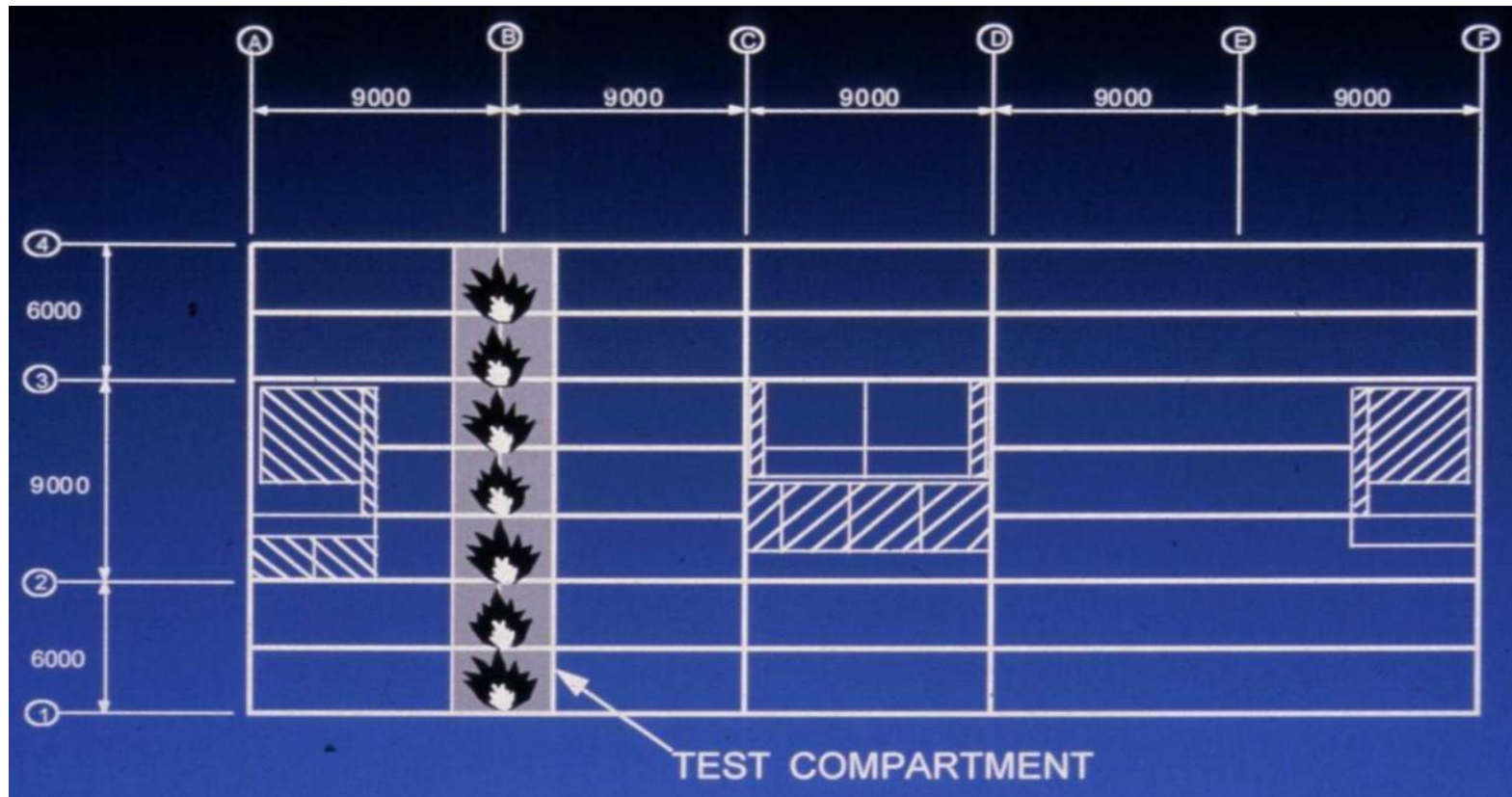


Cardington



Primary beams along the whole object

- Heating by gas burners according to standard temperature time curve

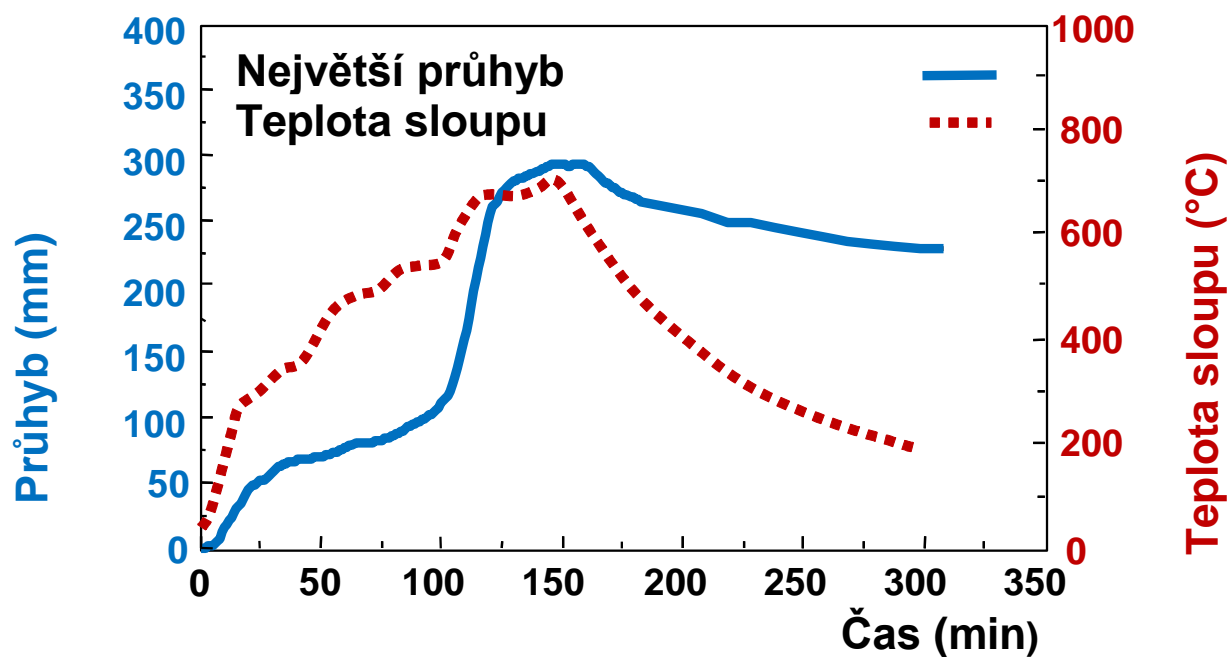


Cardington



Primary beams along the whole object

- Results
 - Max. temperature of the beam 750 °C
 - Beam deflection \approx 300 mm



Cardington



Primary beams along the whole object

- Beams deflection



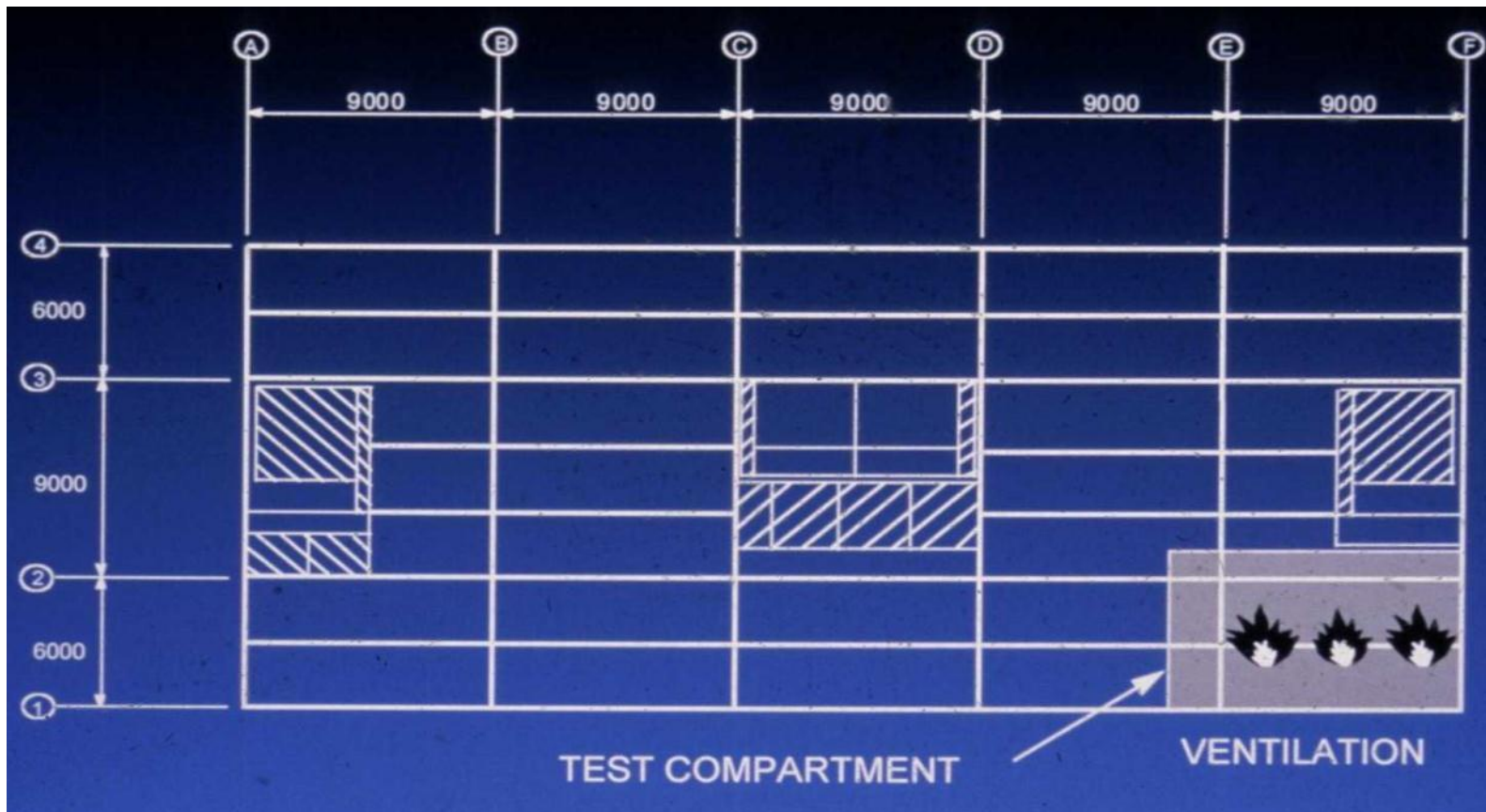
- Deformation of the column

Cardington



Fire compartment in the corner of the object

- Fire load – wooden cribs



Cardington



Fire compartment in the corner of the object

- Before the test

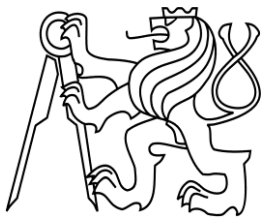


Walls of the fire compartment

Fire load of 45 kg/m²



Cardington



Fire compartment in the corner of the object



During the fire test

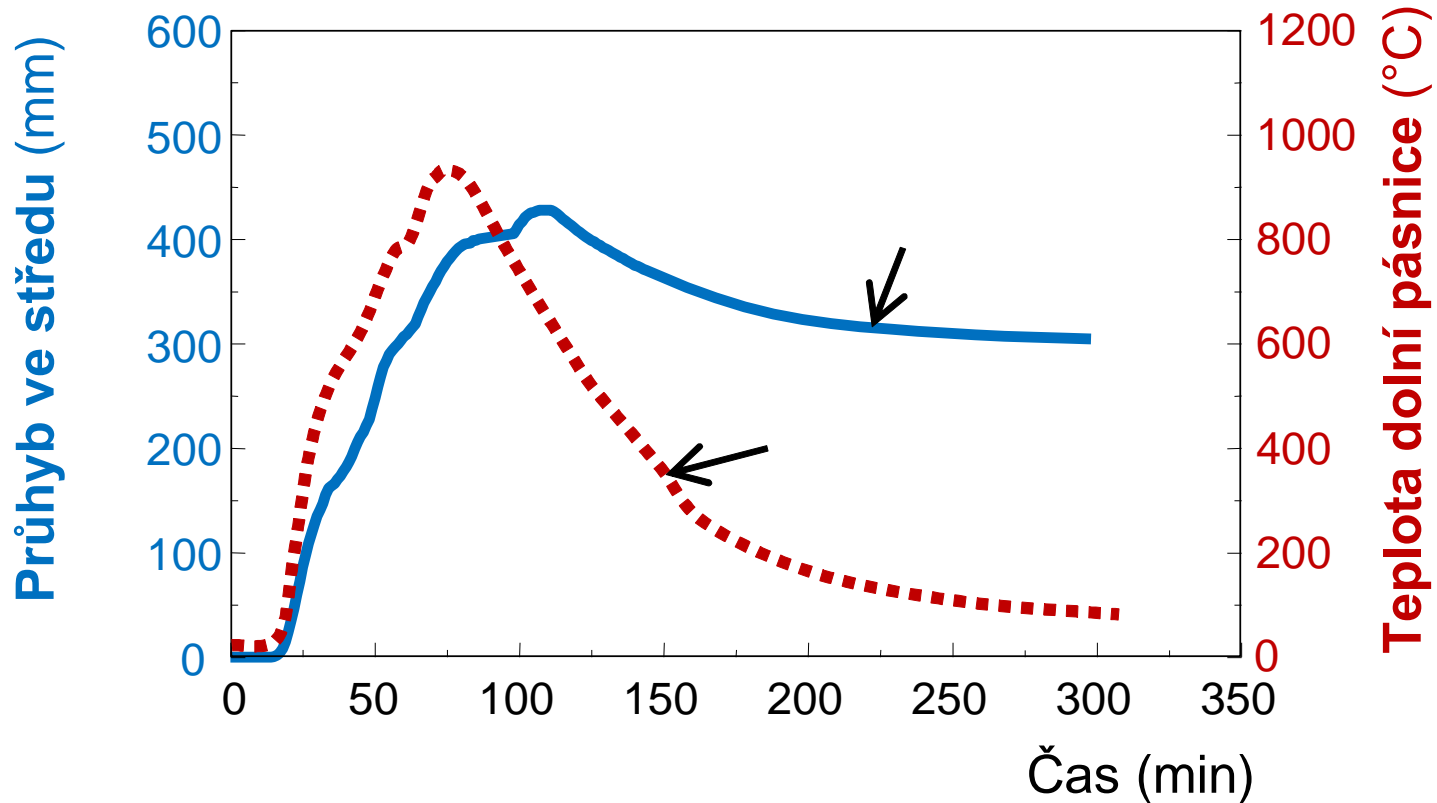
Fire load after the test



Cardington



Fire compartment in the corner of the object



- Lower flange beam temperature 1014 °C
- Deflection in the middle of the span over 428 mm

Cardington



Fire compartment in the corner of the object

- Structure after the fire test



Deformation of the floor slab



Beams around the fire protected column

- **Conclusions**
 - Failure of the structure was not observed, only heating and deformation of members

Cardington

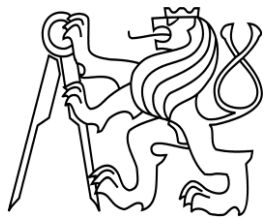


Demonstration fire test

- Floor area of the fire compartment 130 m²
- Fire load – office furniture, computers, papers



Cardington



Demonstration fire test

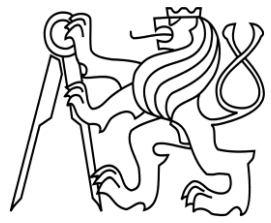


Fire load

Windows with glass



Cardington



Demonstration fire test



Beginning of the fire

Fully-developed fire

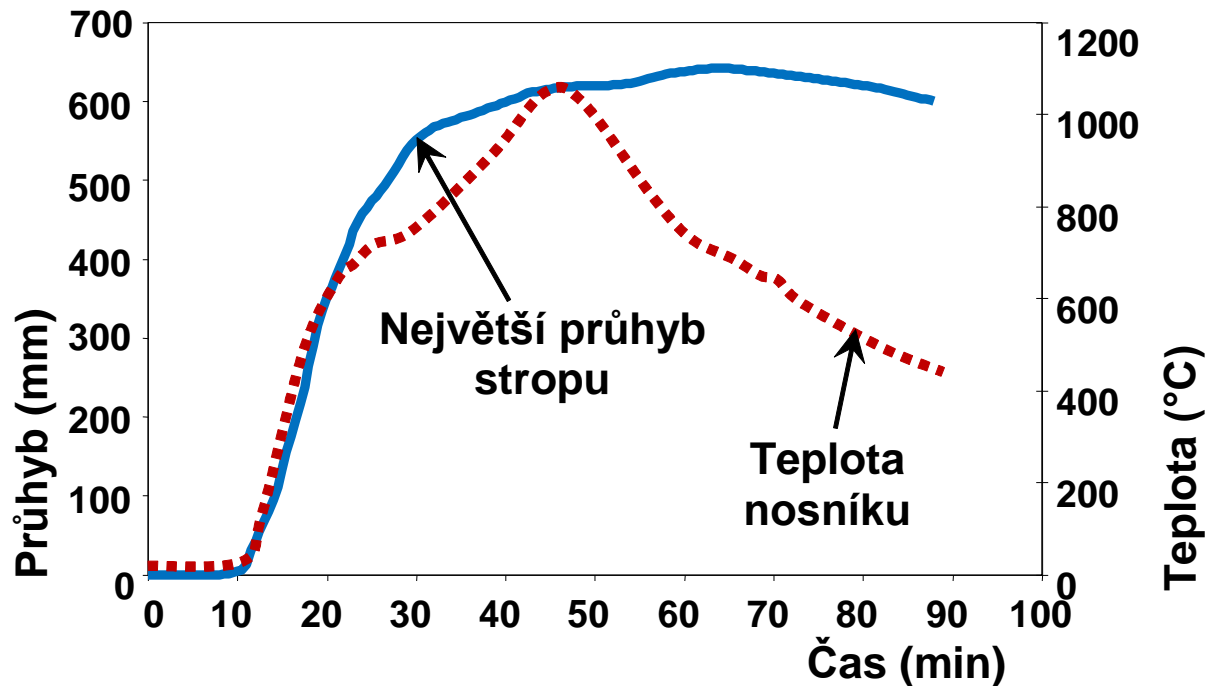


Cardington



Demonstration fire test

- Results



- Observation

- Floor slab deformation ≈ 640 mm
- No brekage of integrity

Cardington

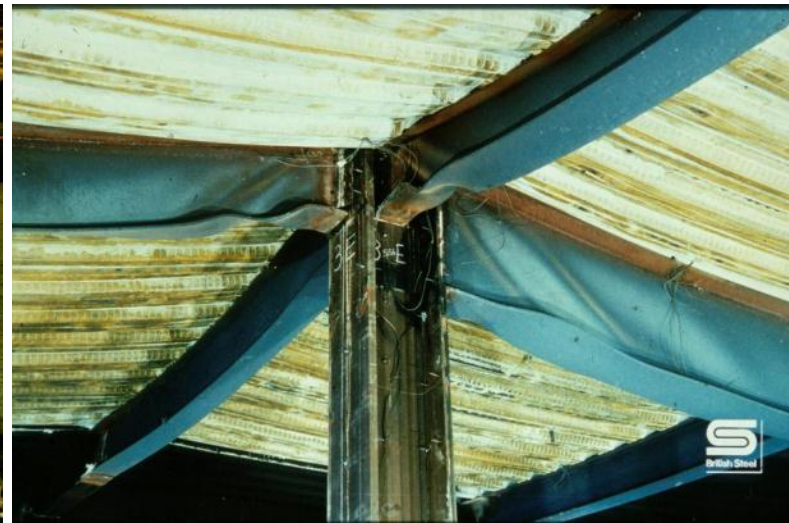


Demonstration fire test

- After the fire test
- No loss of integrity of the structure, no failure

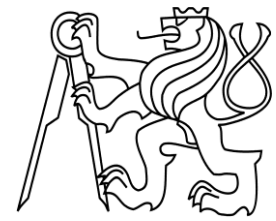


Secondary beam deflection
640 mm



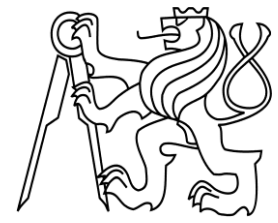
Connection to column

Cardington



- Findings
 - On the structure of steel-concrete composite building there were 7 full-scale tests – no failure of the structure
 - Behaviour of the structure is better than behaviour of the separated members
 - Floor slab could resist to temperatures over 1000 °C
 - During big deflections a membrane effect was observed
 - Floor slab kept its integrity

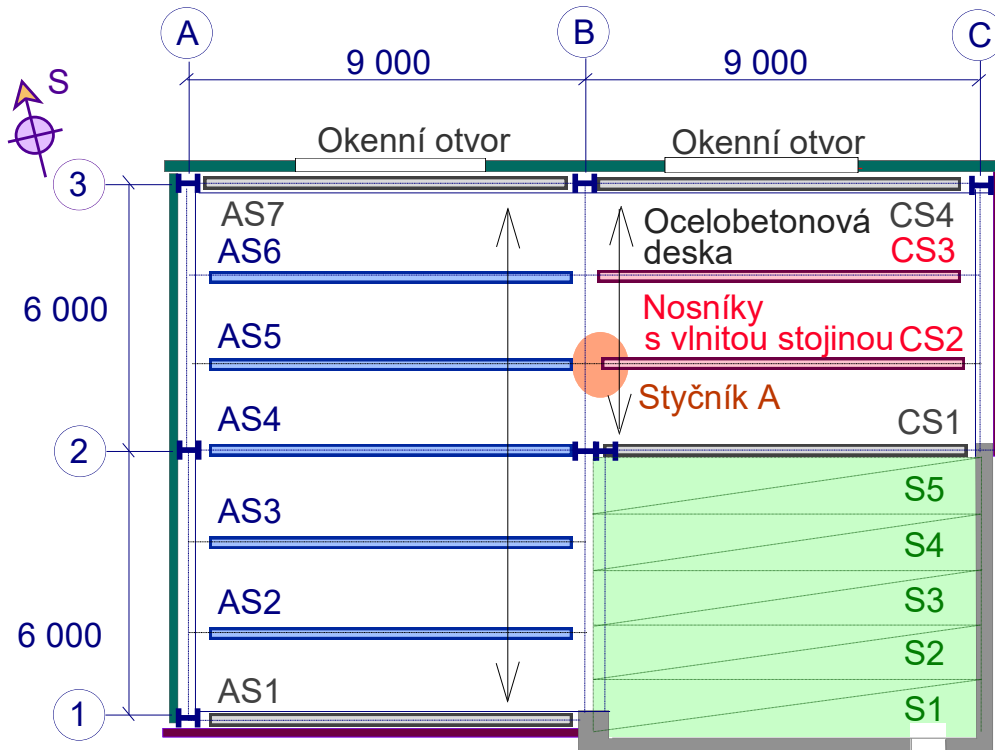
Mokrsko



- CTU fire test in 2008

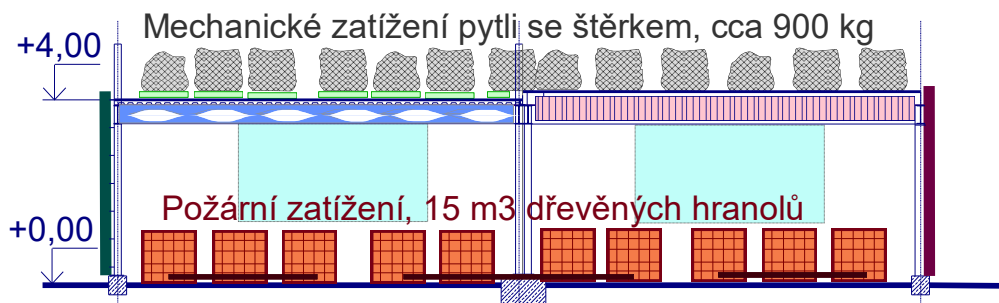


Mokrsko



Load:
mechanical
 $q_k = 3,25 \text{ kN/m}^2$,
Dead weight of the slab
 $g_k = 2,60 \text{ kN/m}^2$

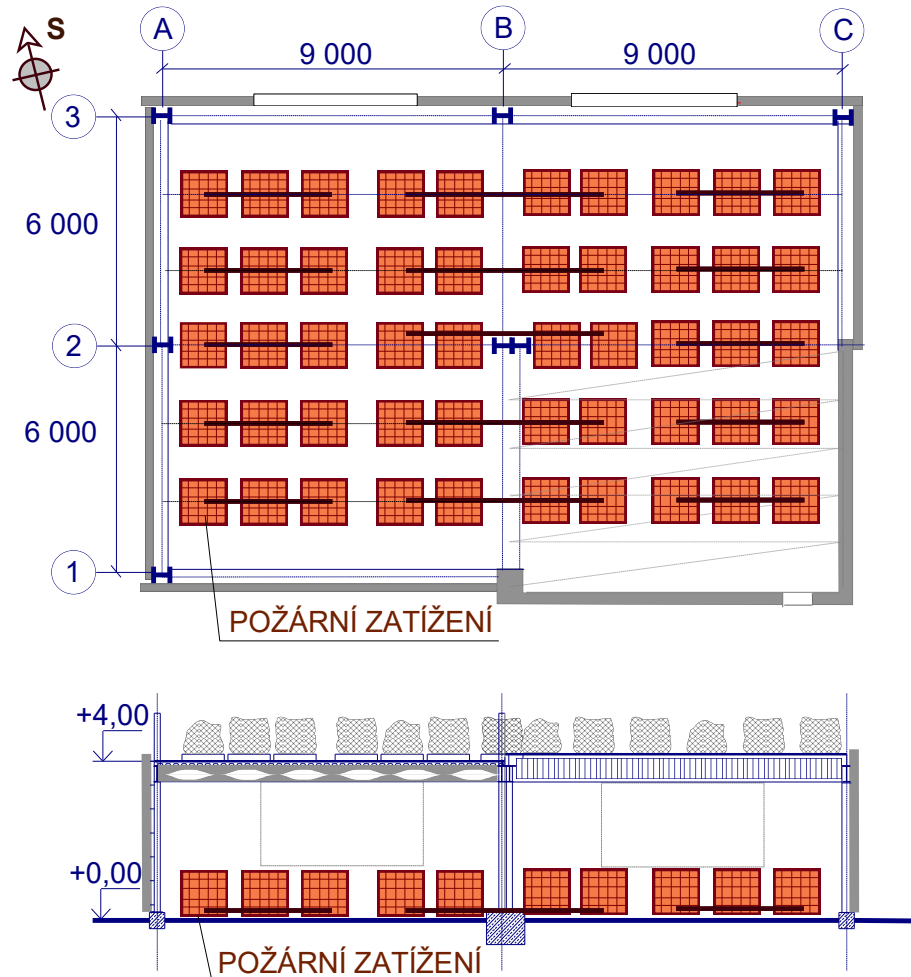
Internal forces at beam CS2
during the fire test:
 $M = 119,8 \text{ kNm}$,
 $V = 53,24 \text{ kN}$



Mokrsko



- Fire load – wooden cribs, 35,5 kg/m²



Mokrsko



- Fire load – wooden piles, 35,5 kg/m²



Mokrsko



- Bearing structure



- Beams with corrugated web, cellular beams (Angelina)
- Composite steel-concrete floor
- Concrete SPIROL panels

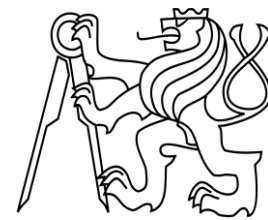
Mokrsko



- Measuring of temperature of the structure



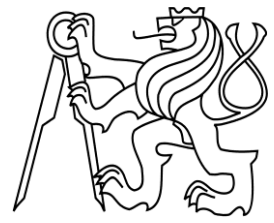
Mokrsko



- During the fire test



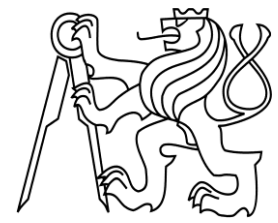
Mokrsko



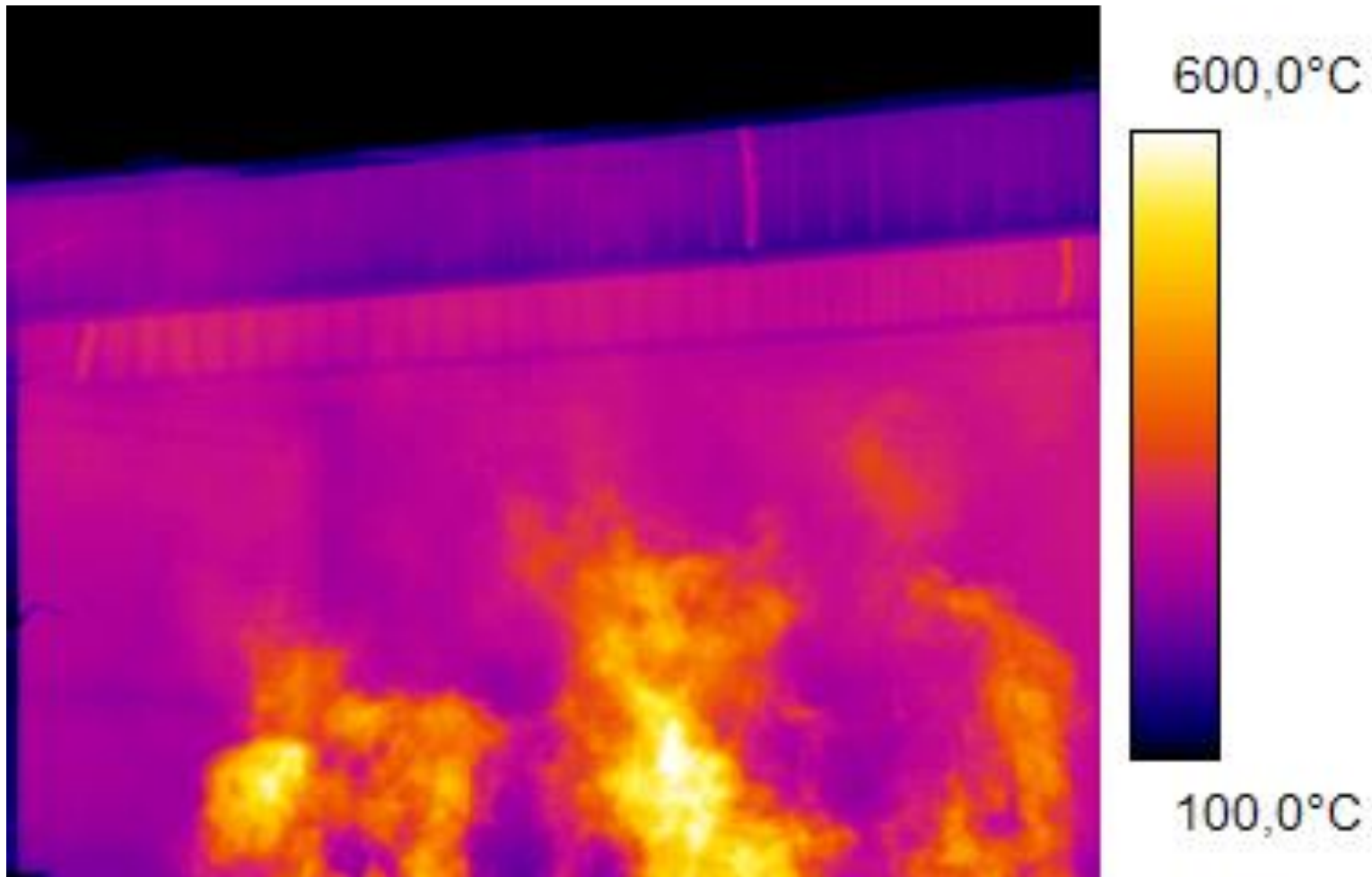
- During the fire test



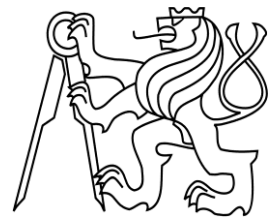
Mokrsko



- Measurement with thermocamera



Mokrsko



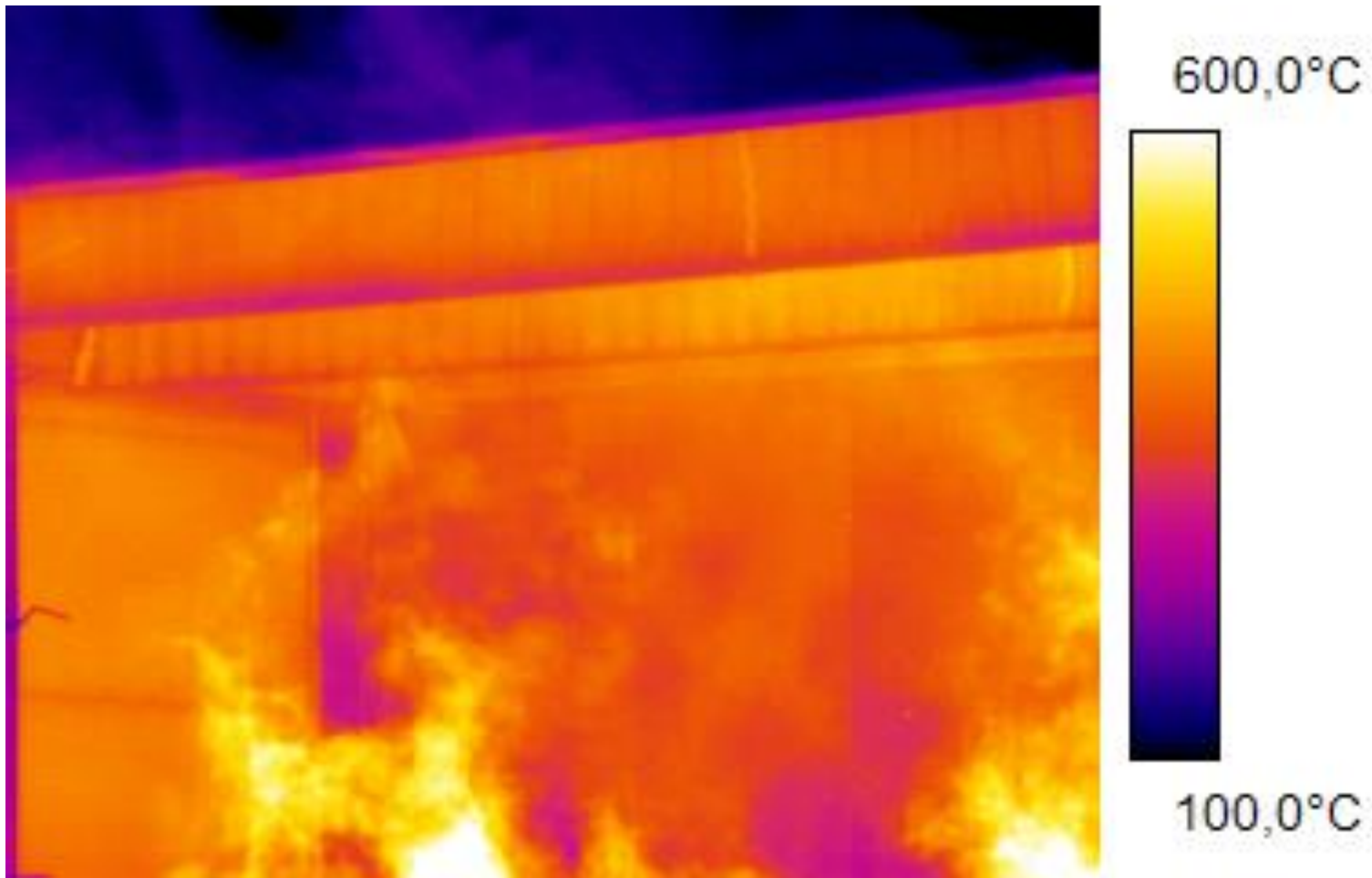
- Fully-developed fire



Mokrsko



- Measurement with thermocamera



Mokrsko



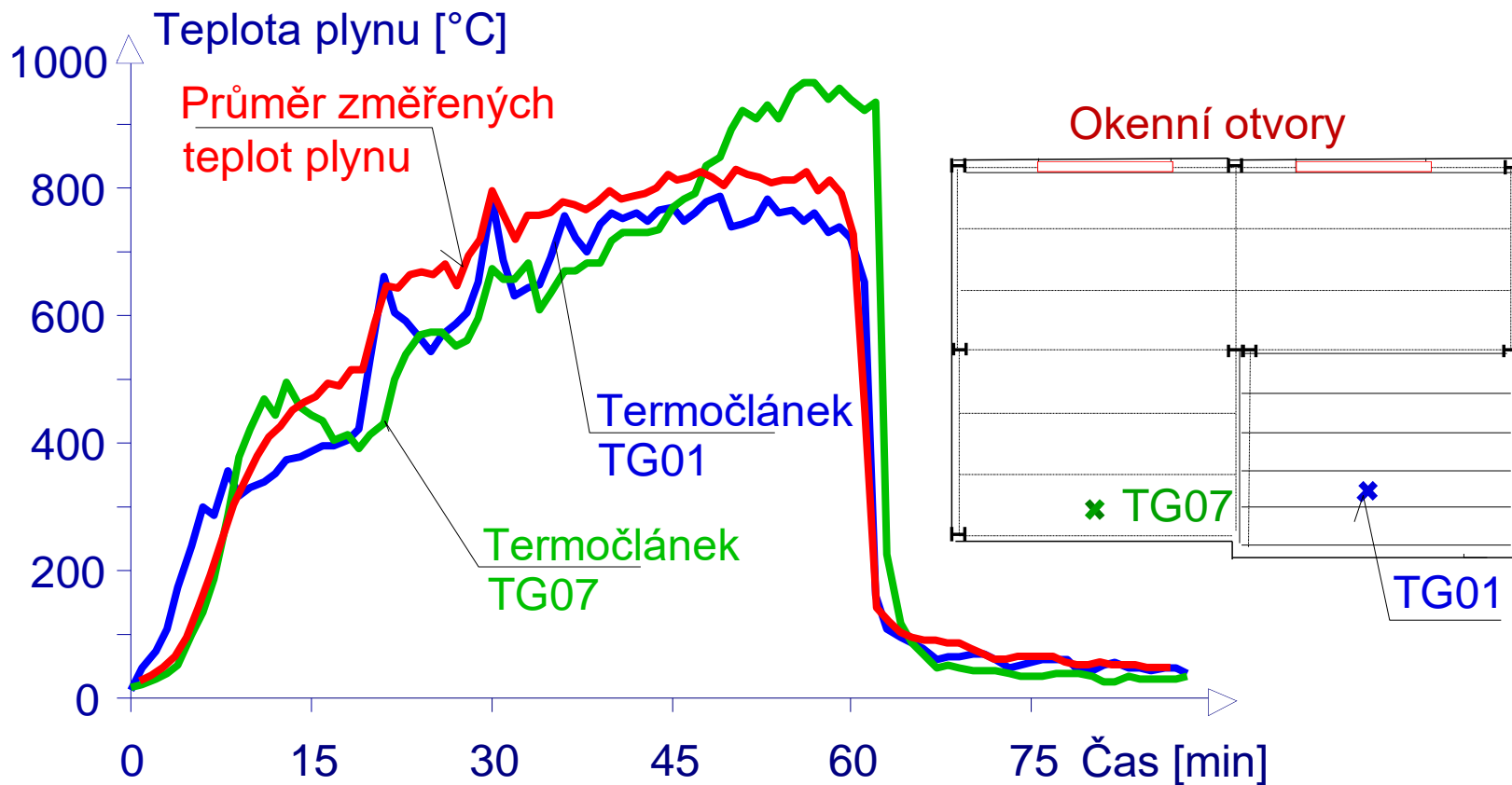
- During the fire test



Mokrsko



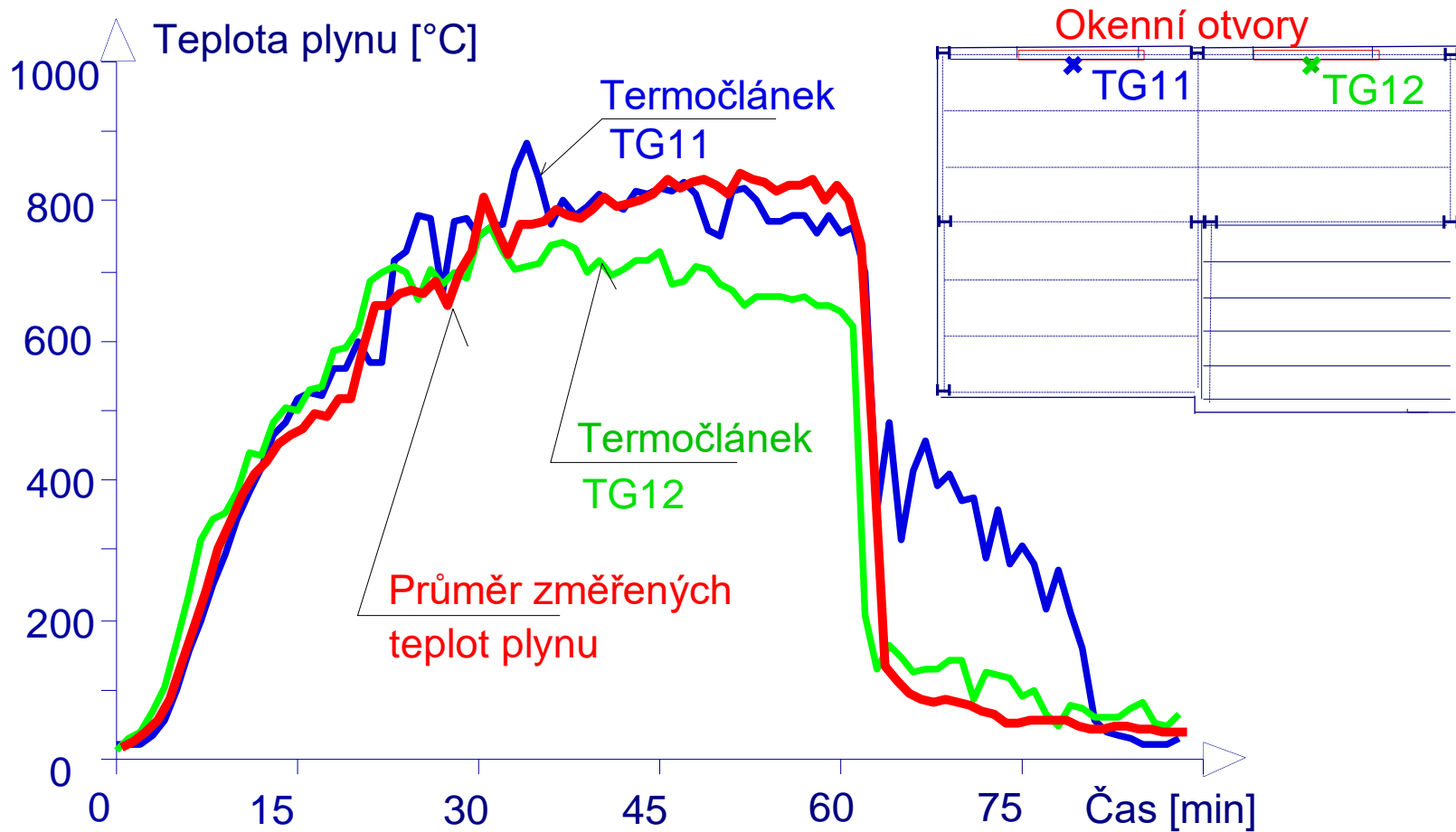
- Gas temperature



Mokrsko



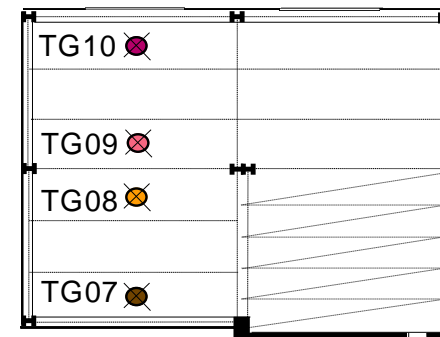
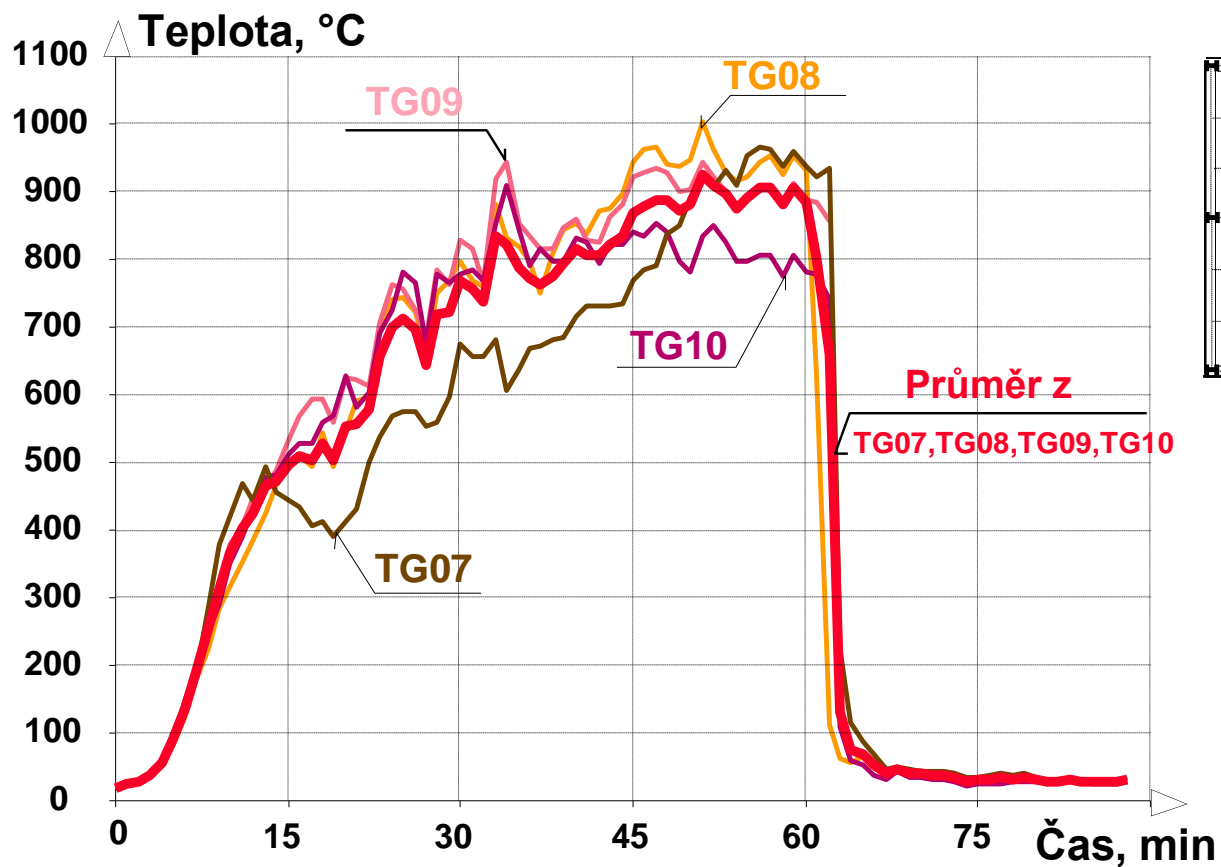
- Gas temperature



Mokrsko



- Gas temperature



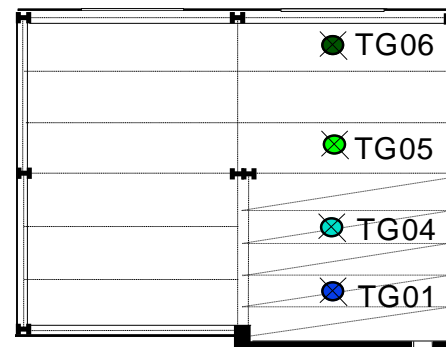
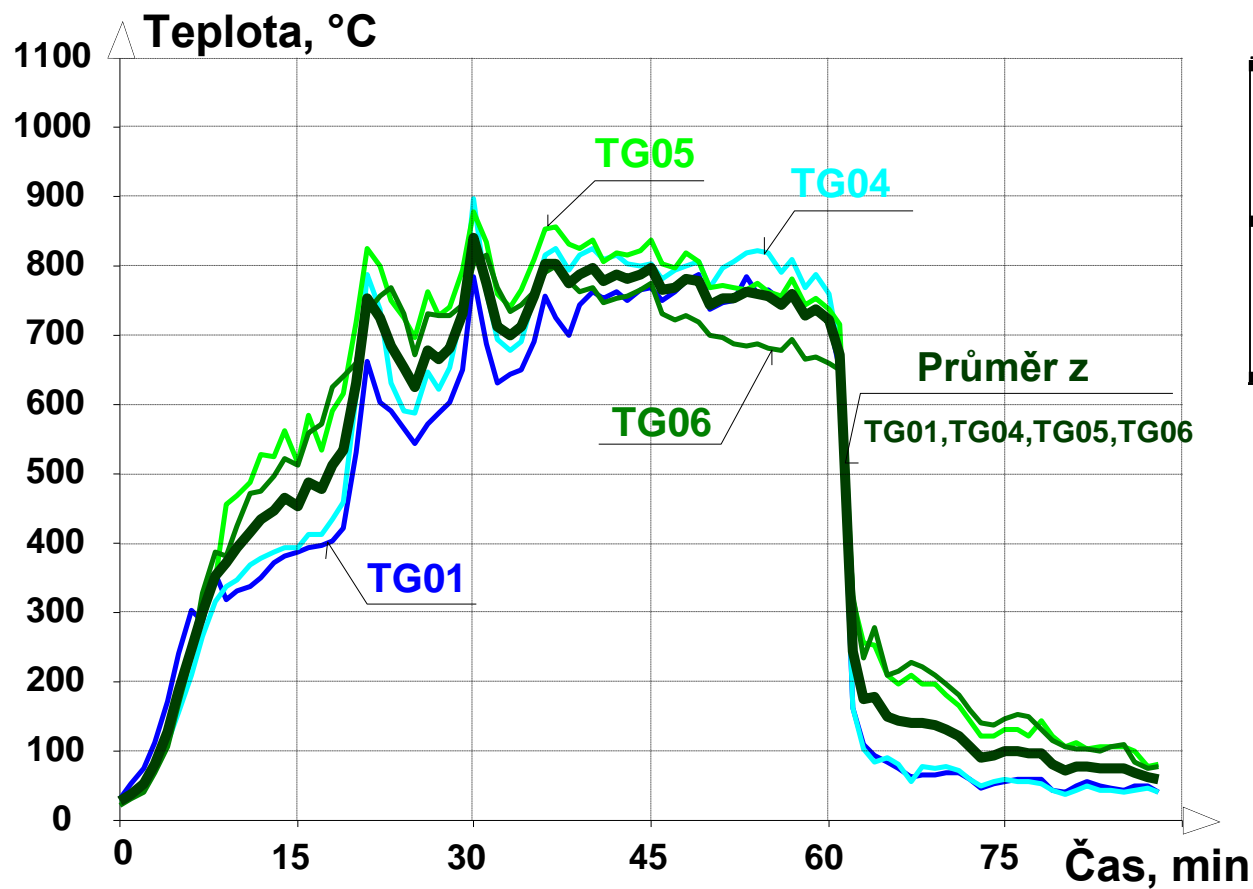
Průměr z

TG07, TG08, TG09, TG10

Mokrsko



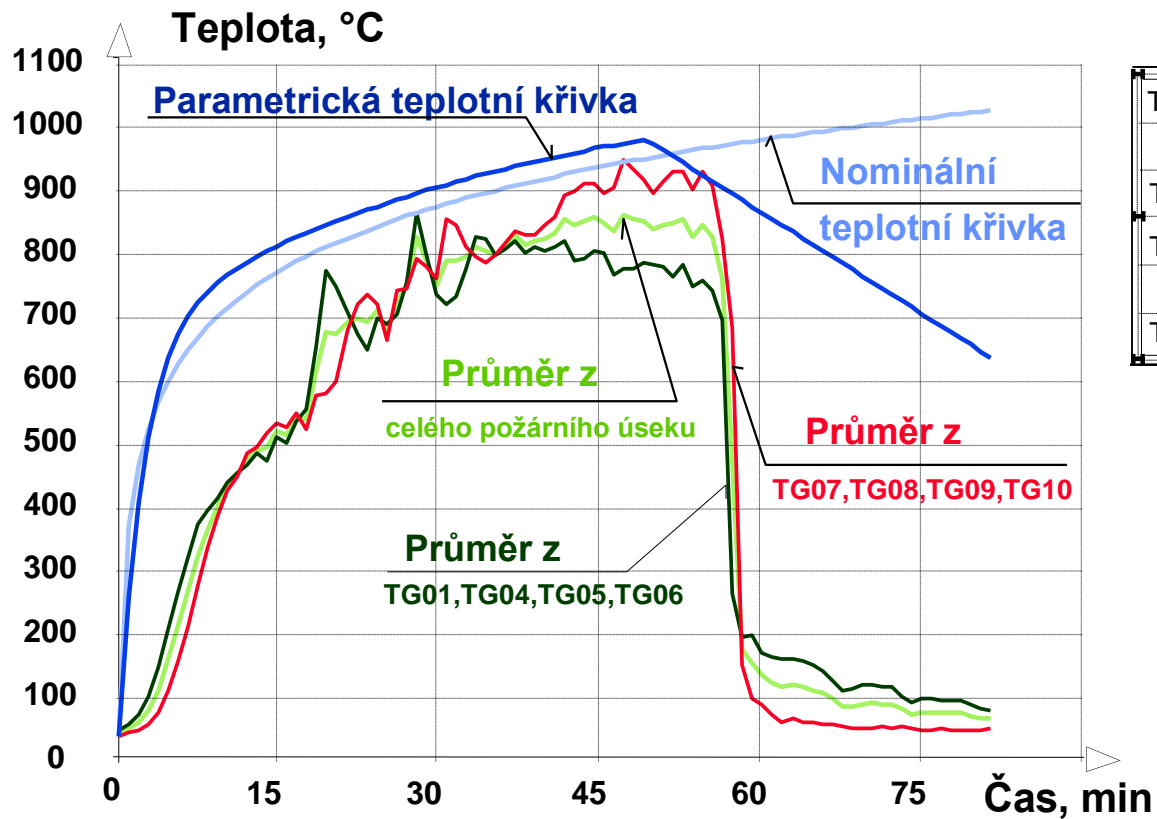
- Gas temperature



Mokrsko



- Gas temperature – comparison to design fire models

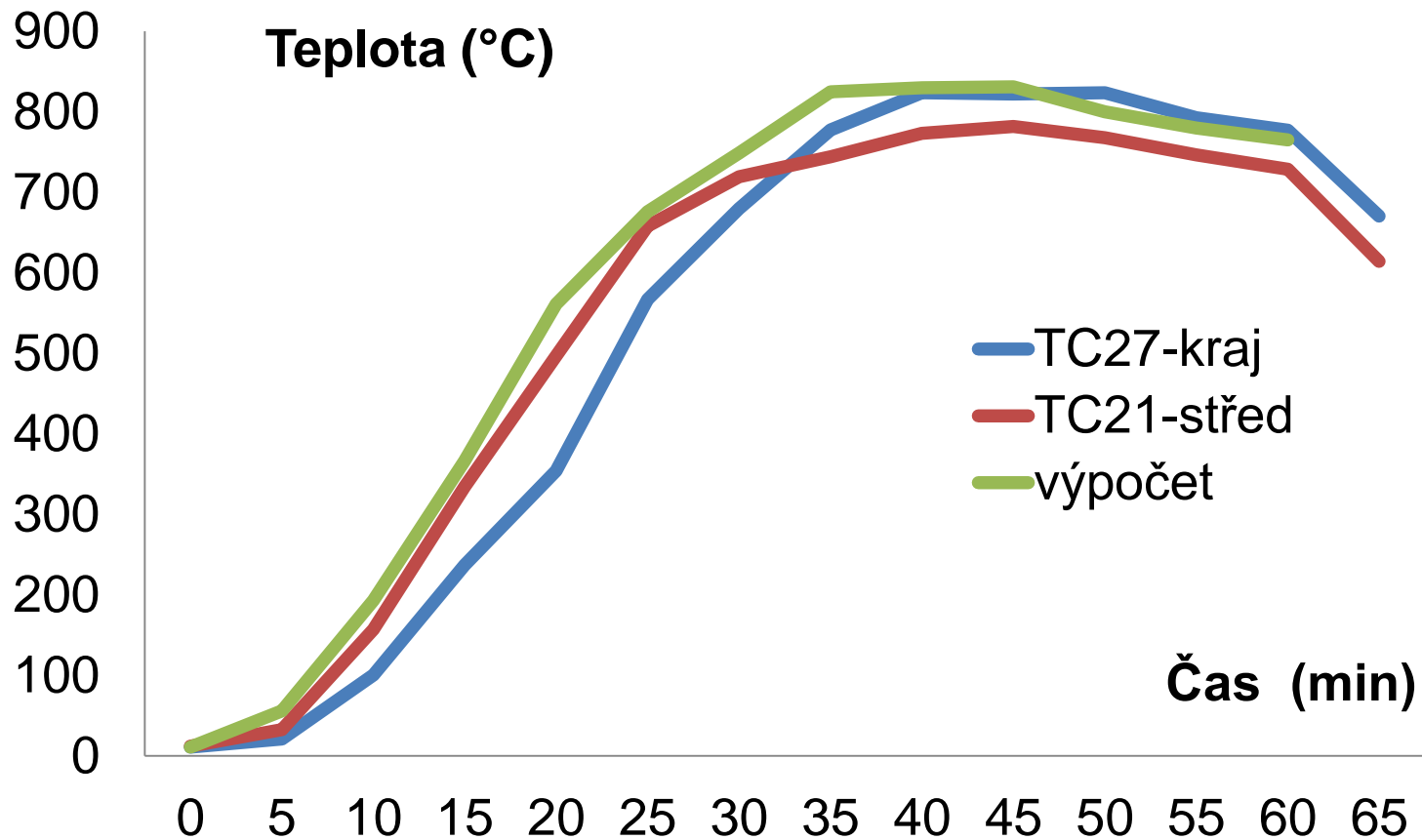


TG10	⊗	TG06	⊗
TG09	⊗	TG05	⊗
TG08	⊗	TG04	⊗
TG07	⊗	TG01	⊗

Mokrsko



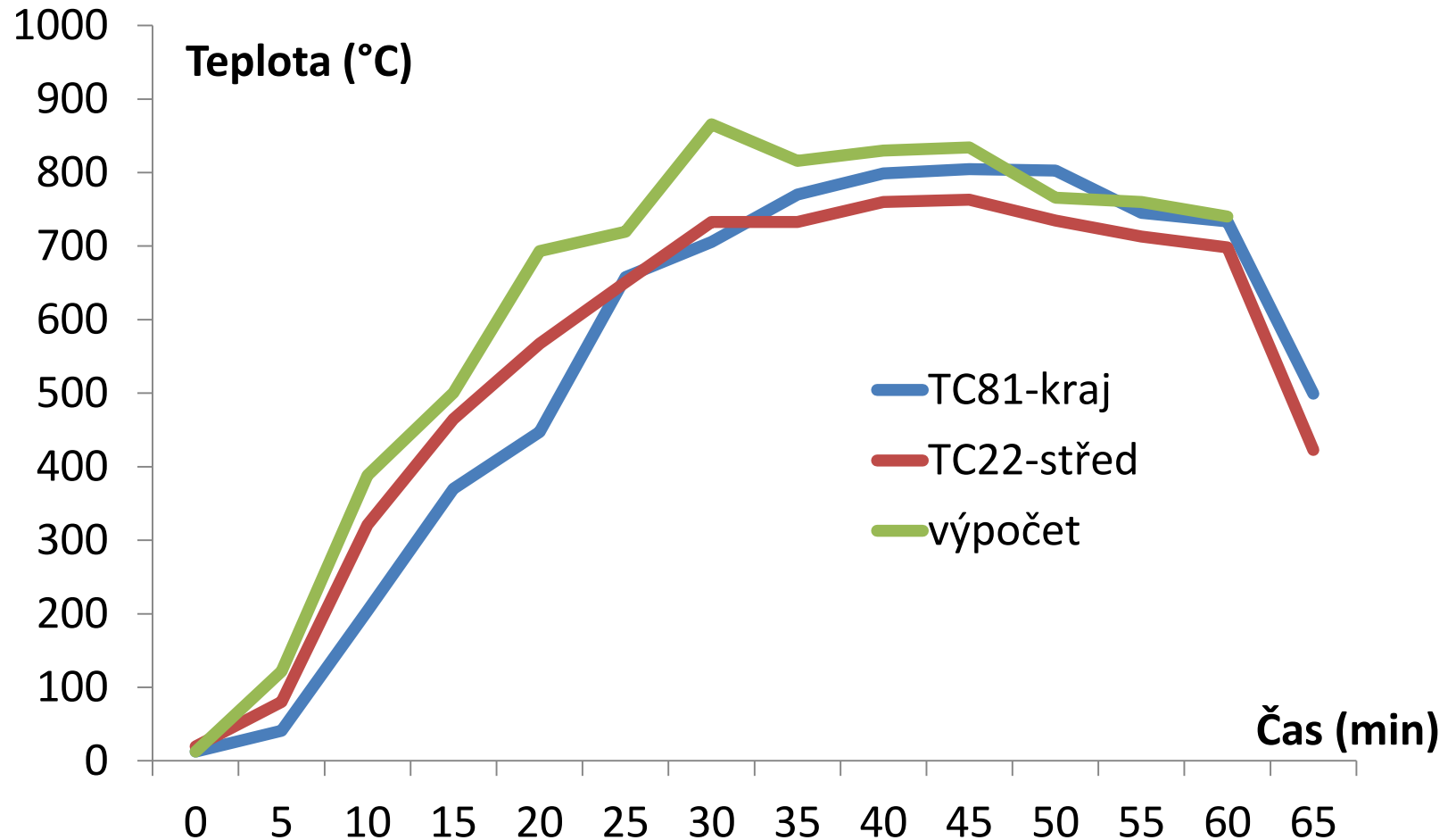
- Temperature of the lower flange of the corrugated beam



Mokrsko



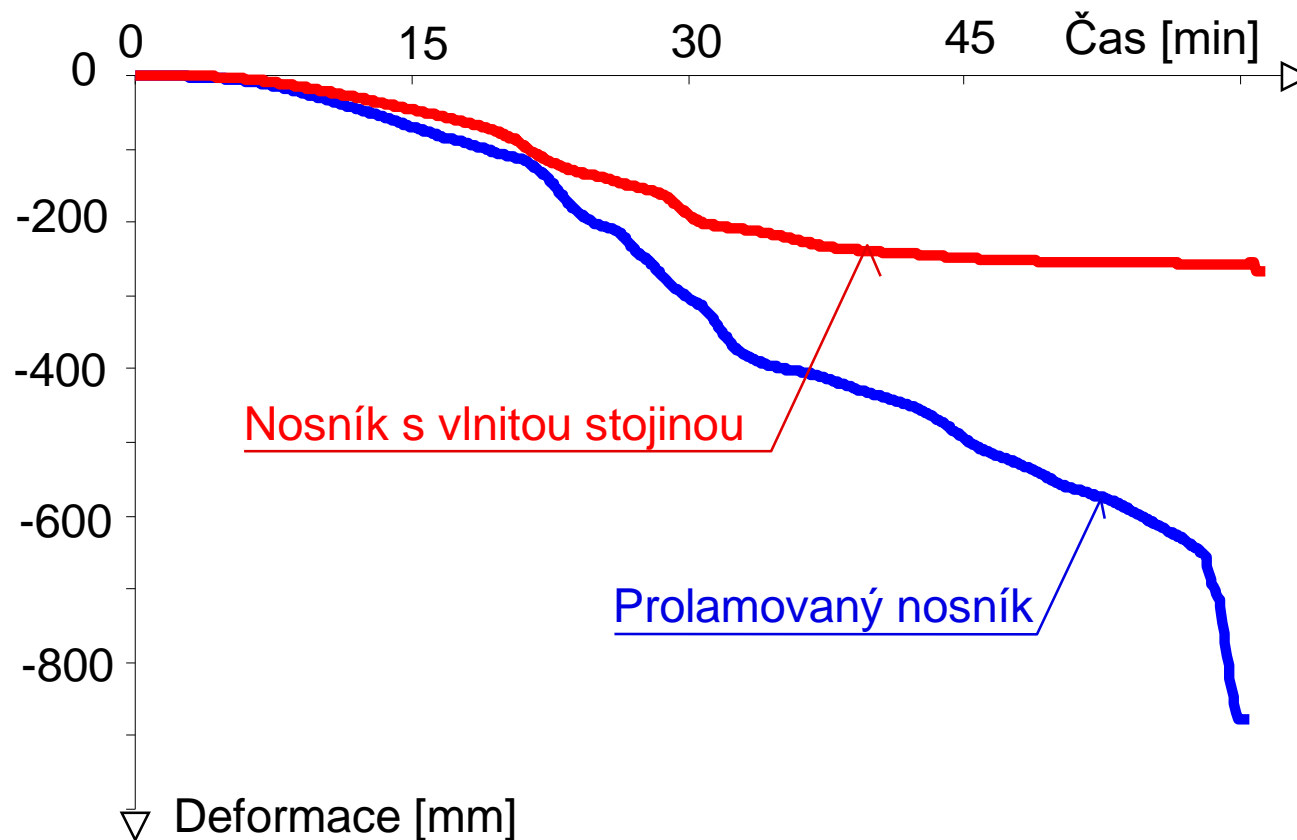
- Temperature of the web of the corrugated beam



Mokrsko



- Deformation of beams



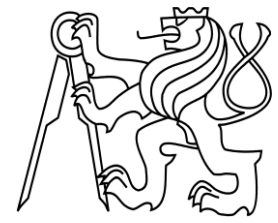
Mokrsko



- Shear deformation of the beam after the test



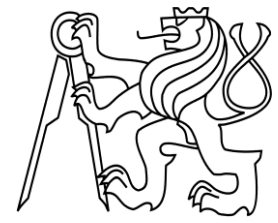
Mokrsko



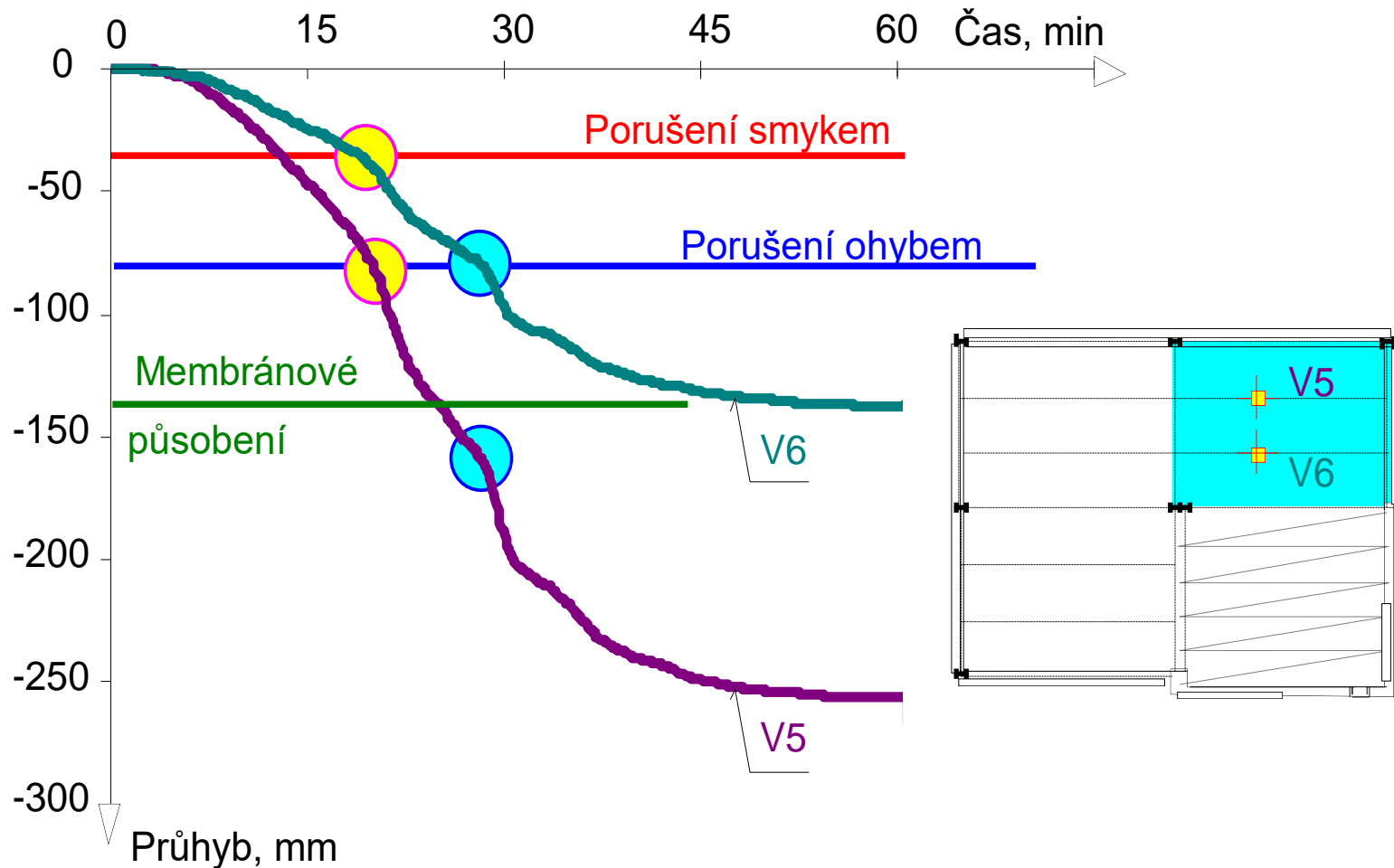
- Shear deformation of the beam after the test



Mokrsko



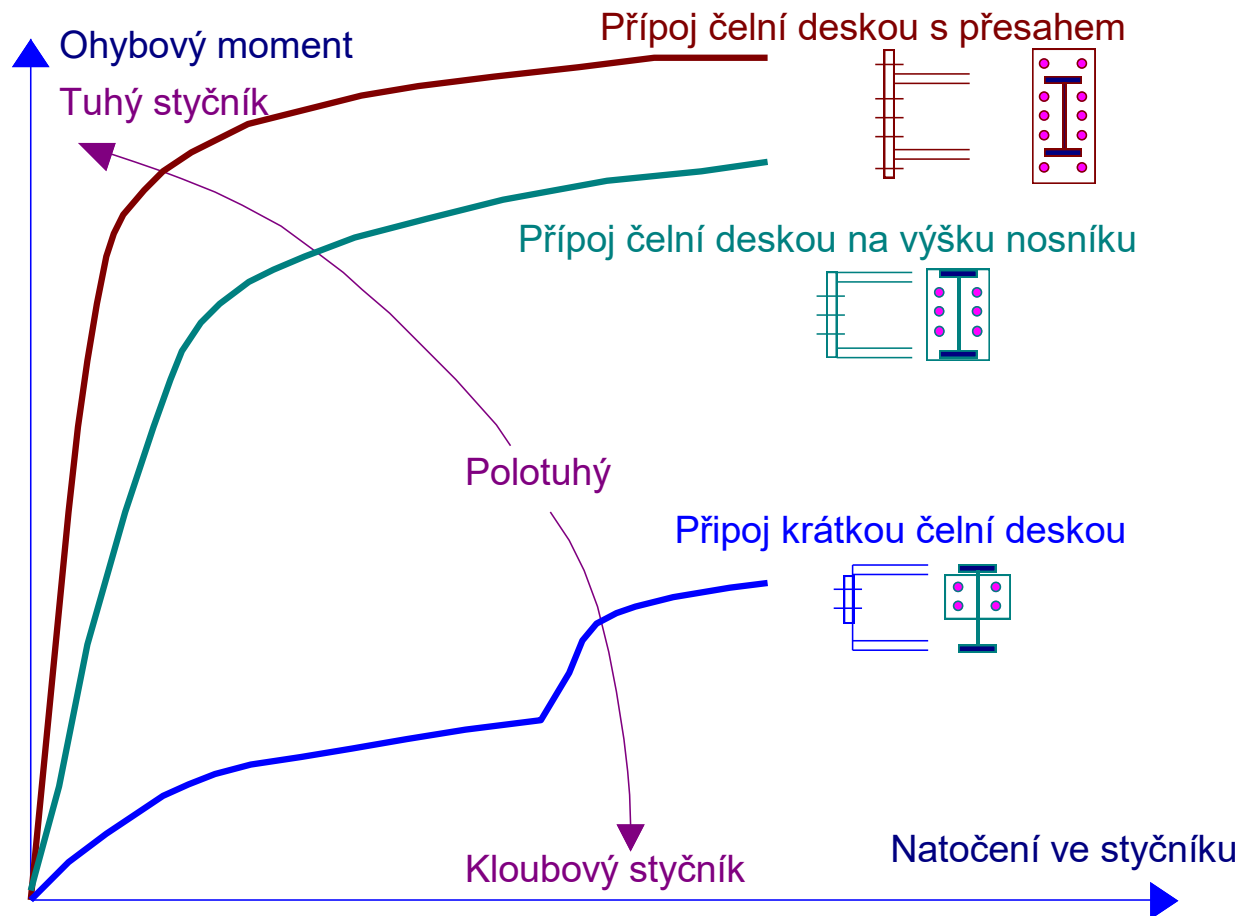
- Deformation of the composite beam



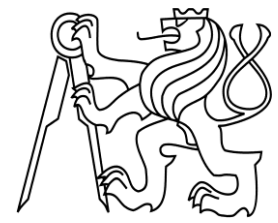
Mokrsko



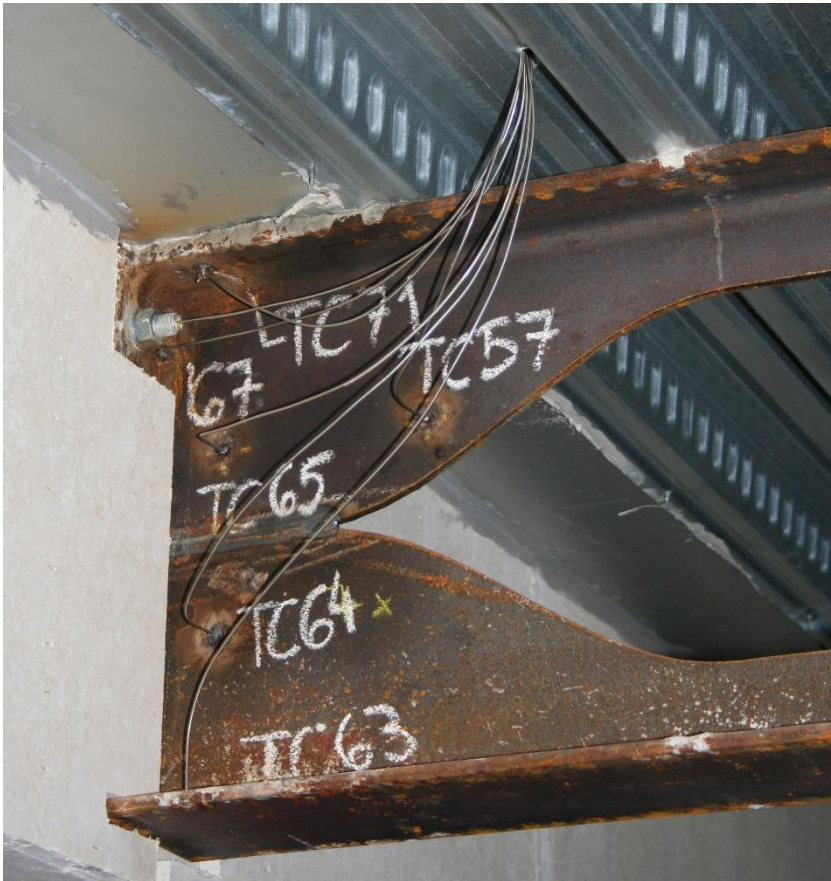
- Connections in the structure



Mokrsko



- Connections after fire



Mokrsko



- Floor slab after the fire test



Veselí n. Lužnicí



- CTU fire test in 2011
- In the upper floor - travelling fire test
- In the lower floor – fully-distributed fire



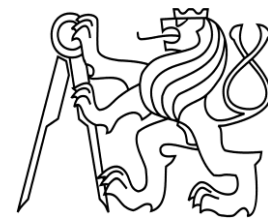
Veselí n. Lužnicí



- Mounting of the structure



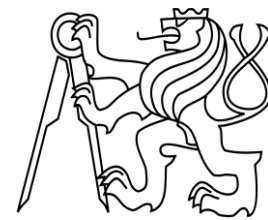
Veselí n. Lužnicí



- Mounting



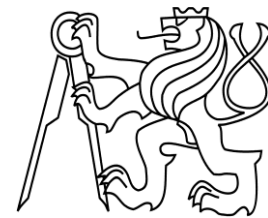
Veselí n. Lužnicí



- Mounting



Veselí n. Lužnicí



- Mounting



Veselí n. Lužnicí



- Mounting



Veselí n. Lužnicí



- Mounting



Veselí n. Lužnicí



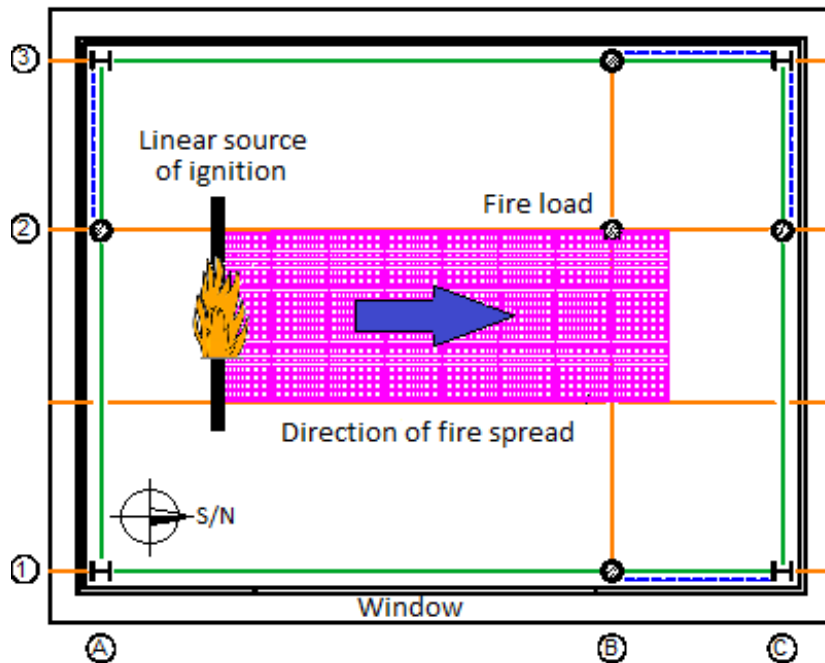
- Mountin



Veselí n. Lužnicí



- Travelling fire



- 10,4 x 13,4 x 4,0 m
- Composite steel-concrete structure
- Opening 2,0 x 5,0 m
- Fire load
 - 24 piles from wooden cribs
 - 2,52 m³ of wood
 - Lineare source of ignition

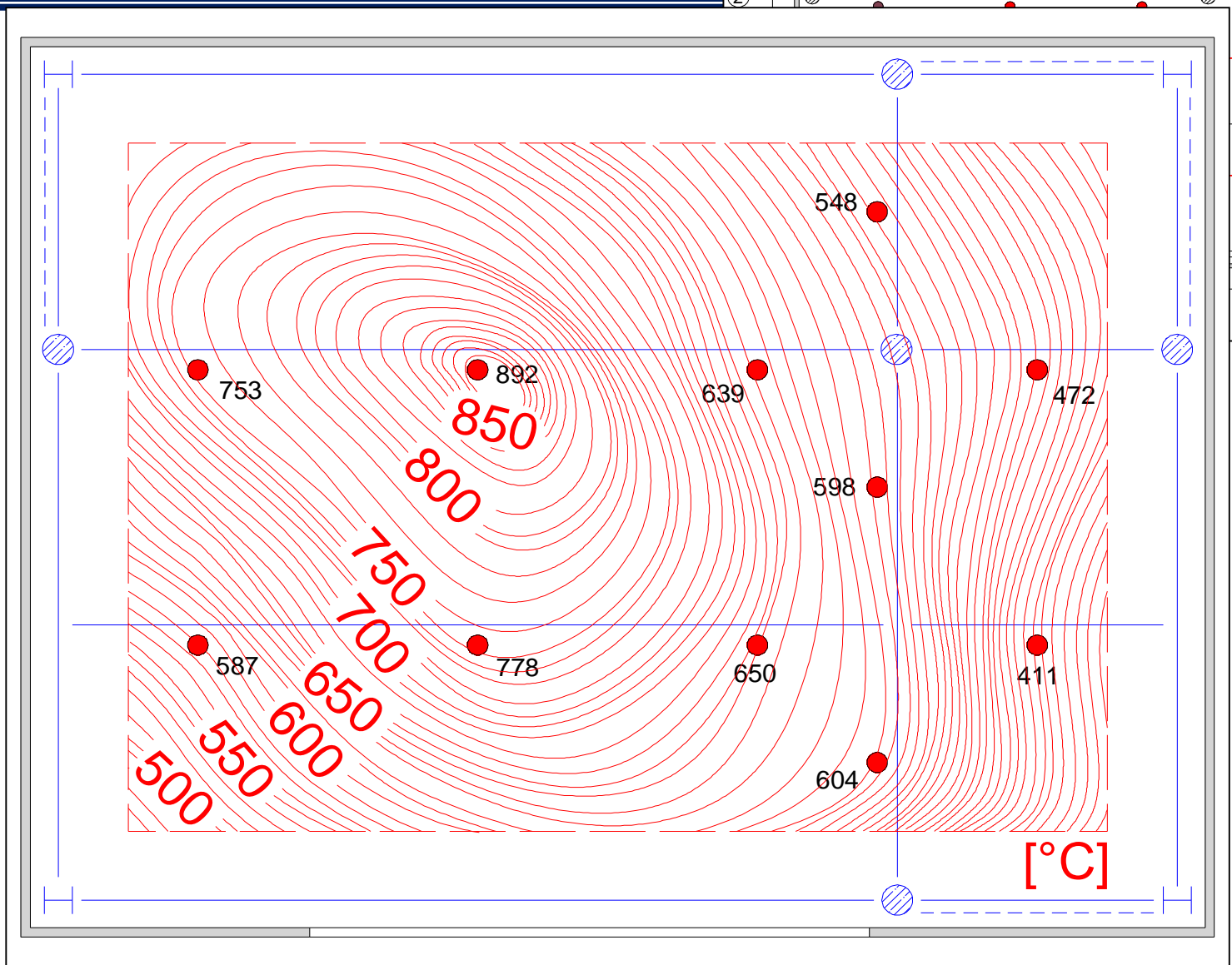
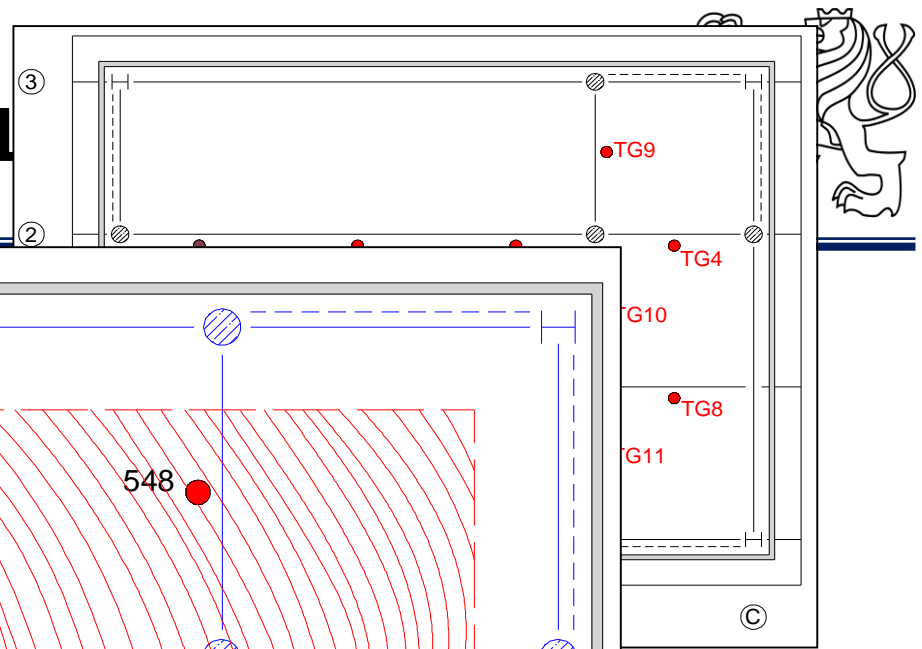
- 20 thermocouples of \varnothing 3 mm
- 7 plate thermometers



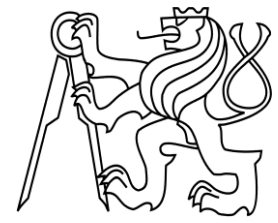
Veselí n. Lužnicí



Veselí n. L



Veselí n. Lužnicí



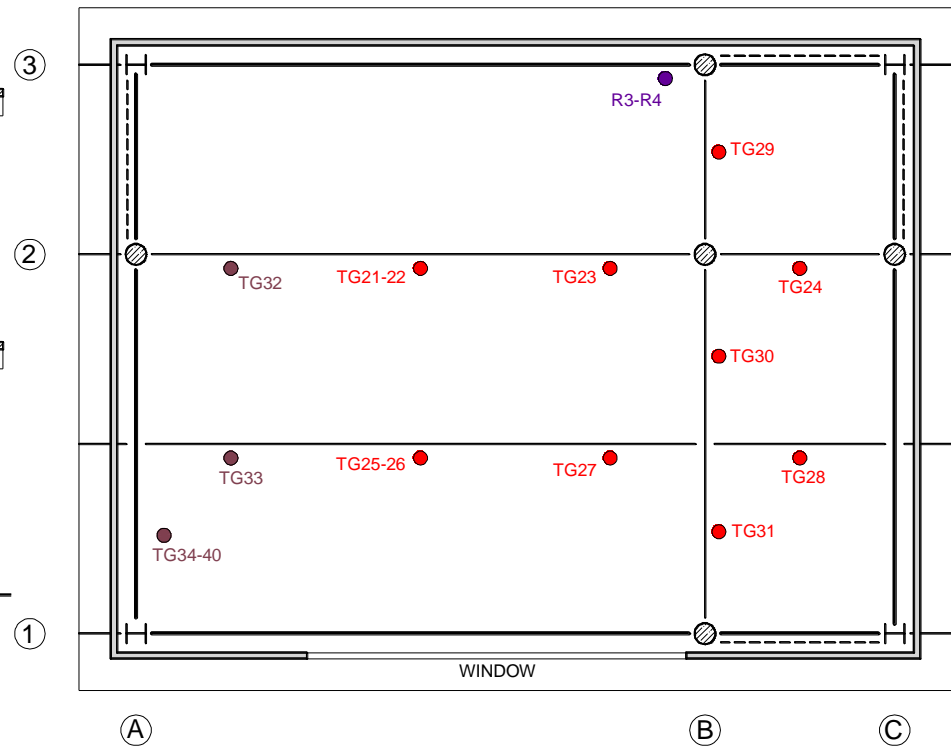
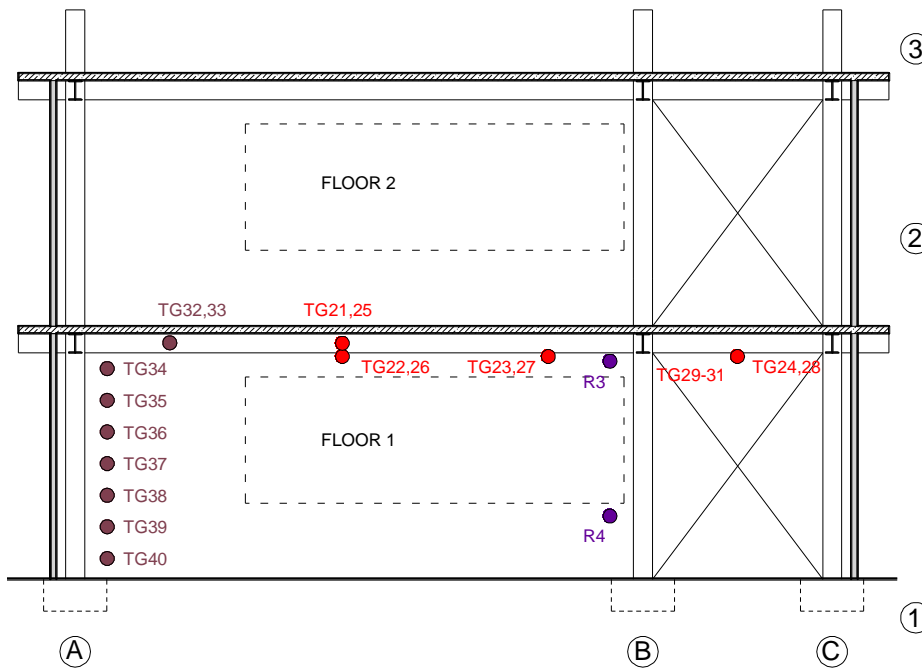
- Fully-distributed fire



Veselí n. Lužnicí



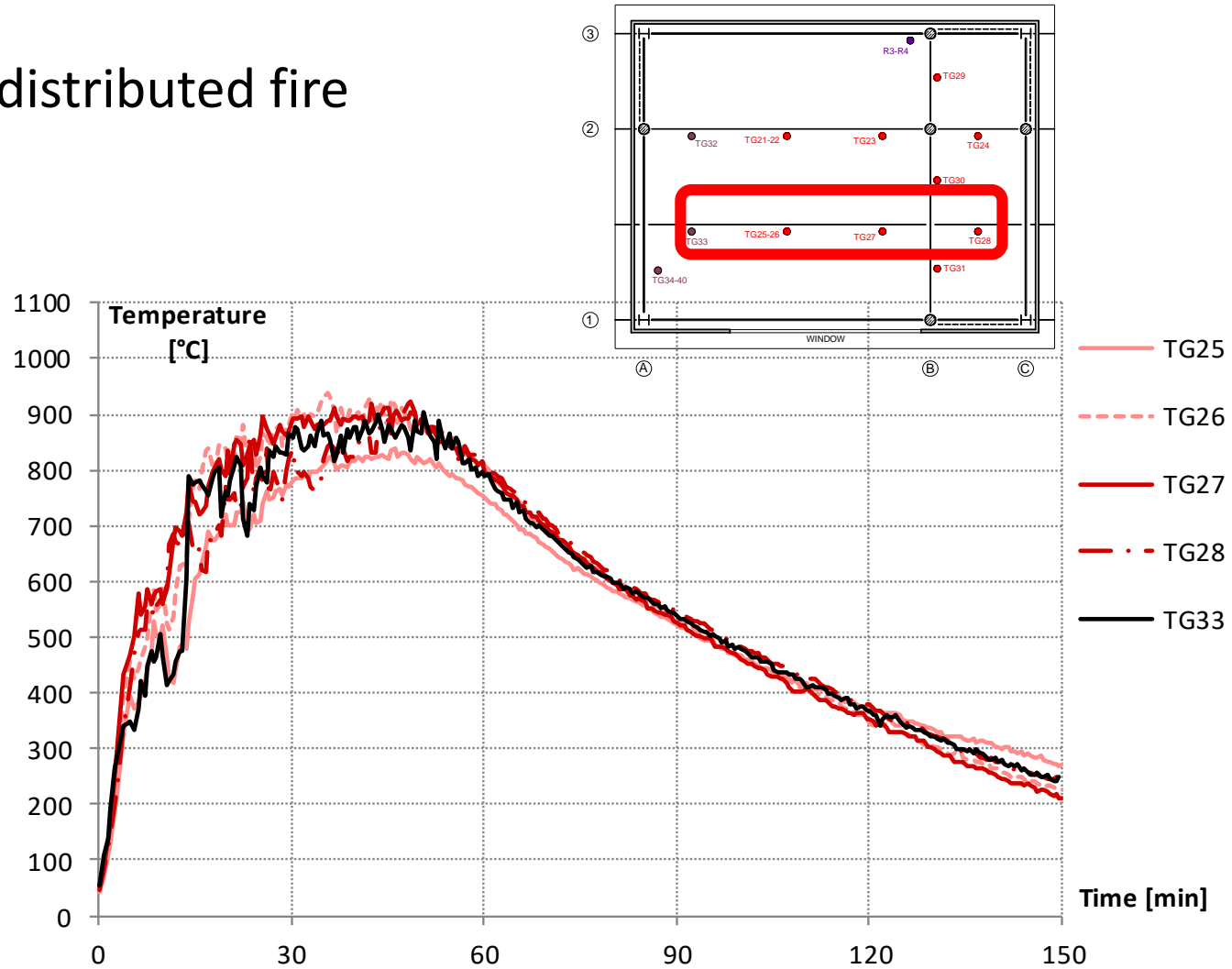
- Fully-distributed fire



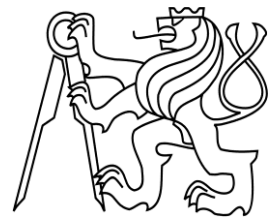
Veselí n. Lužnicí



- Fully-distributed fire



Summary



Full-scale fire tests of structures

- Source of knowledge
- Only for research reasons (cost demands)
- Fire tests:
 - Cardington, Mokrsko, Veselí n.L.
 - Dalmarnock (Glasgow)
 - FRACOF
 - FICEB
 - COSSFIRE
 - etc.



Thank you for your attention!

kamila.cabova@fsv.cvut.cz